

Development of a knee prosthesis powered by electro-hydrostatic actuation

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ISTITUTO
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Doctorate Program Goal

- ▶ Goal:

“Analyze *active* lower-limb prosthetic devices and try to present a novel solution for such systems from a *mechanical design perspective*”

- ▶ In Italy → **11'639** lower limb amputations per year
- ▶ Amputation → great **impairment** to quality of life
 - 67% suffer from Phantom-limb pain
 - 20.6%-60.3% suffer from depressions
 - 25%-57% suffer from anxiety
 - +280% oxygen consumption in above-knee amputation
- ▶ The existing devices are not yet **adequate**
 - 33.87% abandonment rate
 - Difficulties for the user to adapt to such devices
 - Mostly rely on passive or semi-active solutions not-capable of exerting active power



Knee Prostheses – State-of-the-art



Semi-Active Prostheses Electronically-Controlled Damper

- Low functionality
- Light-weight (1.5 – 2 kg)
- Low Energy Consumption
 - Most adopted



Intermediate Solution



- Medium functionality
- Light-medium weight
- Optimized Energy Consumption



- **Efficiency**
- **Integration**
- **Back-drivability**



Fully-Active Prostheses Electro-mechanical Actuation

- High functionality
- Heavy (3.5 – 4 kg)
- High Energy Consumption
 - Most abandoned

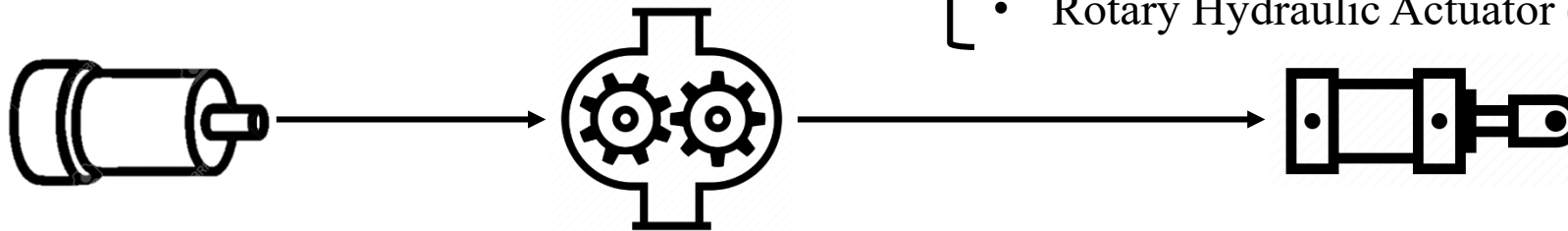
Proposed Architecture: Electro-hydrostatic Actuation (EHA)

- ▶ Alternative to classical electro-mechanical actuation

- ▶ Architecture:

- Electrical Motor → Hydraulic Pump →

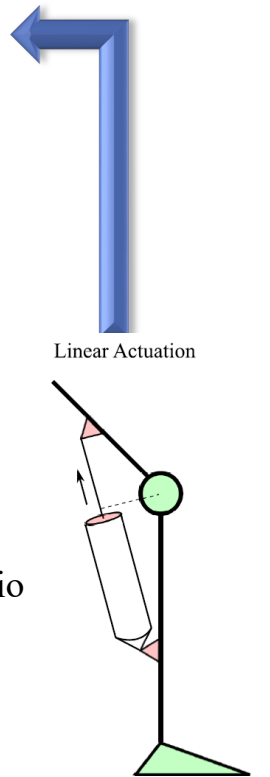
- Linear Hydraulic Cylinder (linear-EHA)
- Rotary Hydraulic Actuator (rotary-EHA)



- ▶ Main Advantages (known from literature):

- Good controllability
- High back-drivability
- Good power-to-weight ratio

- Better Mass Distribution
- Angle-Dependent – Transmission Ratio



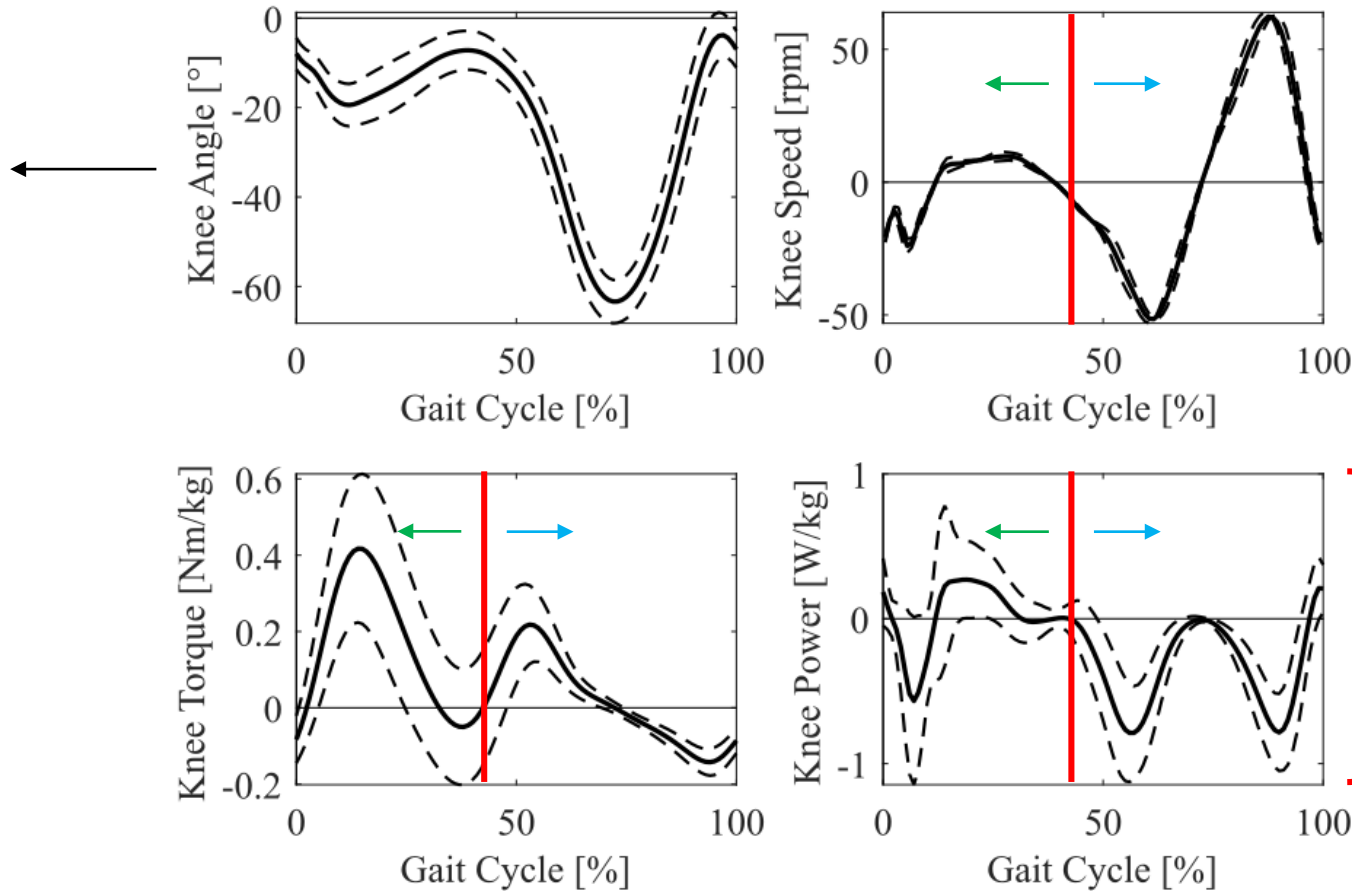
Knee Biomechanics

▶ Actuator Designed to satisfy **Level Walking Requirements**

High Torque – Low Speed Low Torque – High Speed

Range of Motion
(ROM) $\geq 65^\circ$

Selected ROM: 110°



Knee Works Mainly as a Brake:

- Negative Mean Power

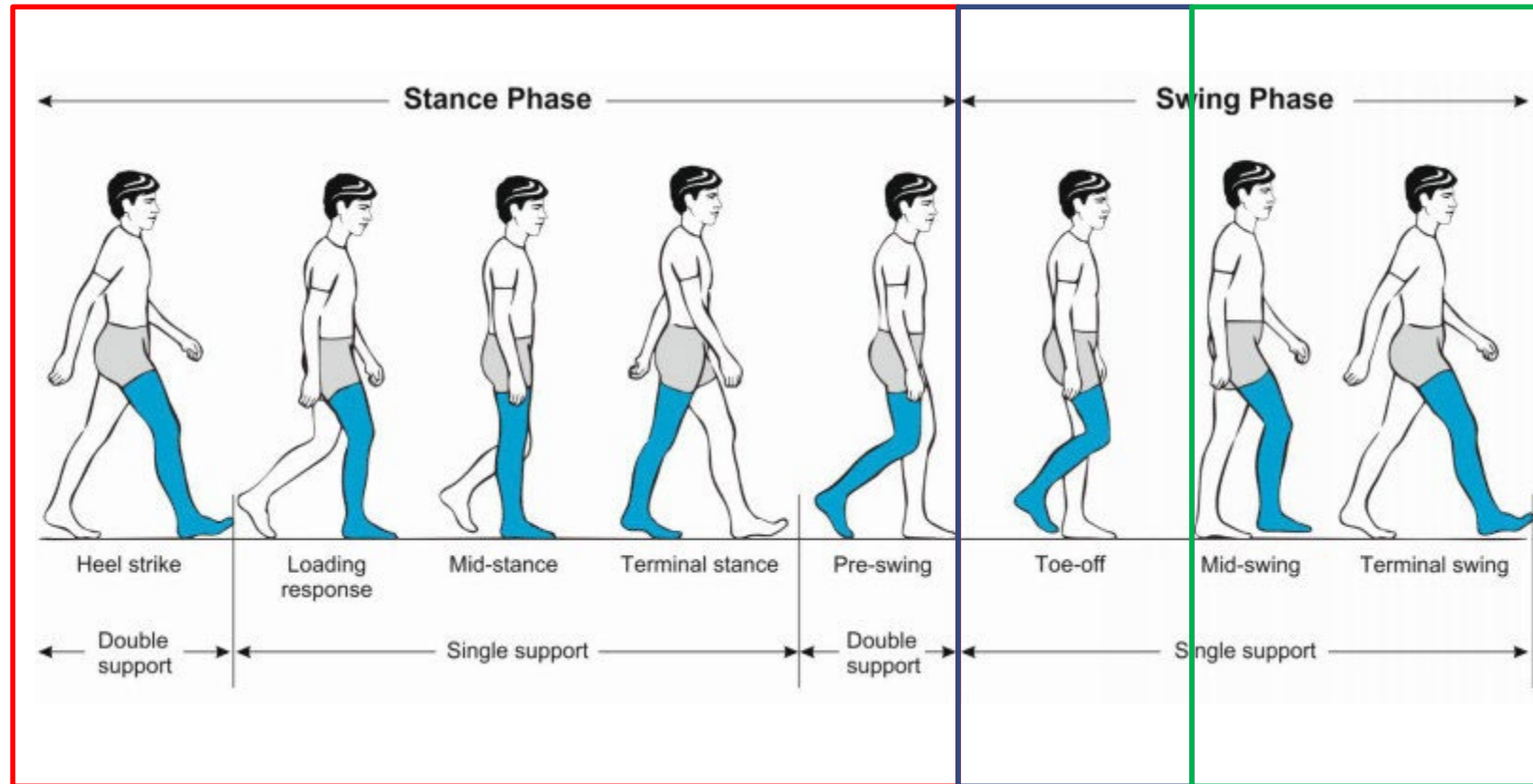
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Power Regeneration Possibility

Gait Cycle – Level Walking

Mostly Active behavior

Passive braking behavior

Knee behaves as a Spring-Damper system → **Admittance Control** in the lower leg → **Regenerative braking**



Partially Active behavior

Knee flexes the lower leg → **Position Control**

Actuation Kinematics

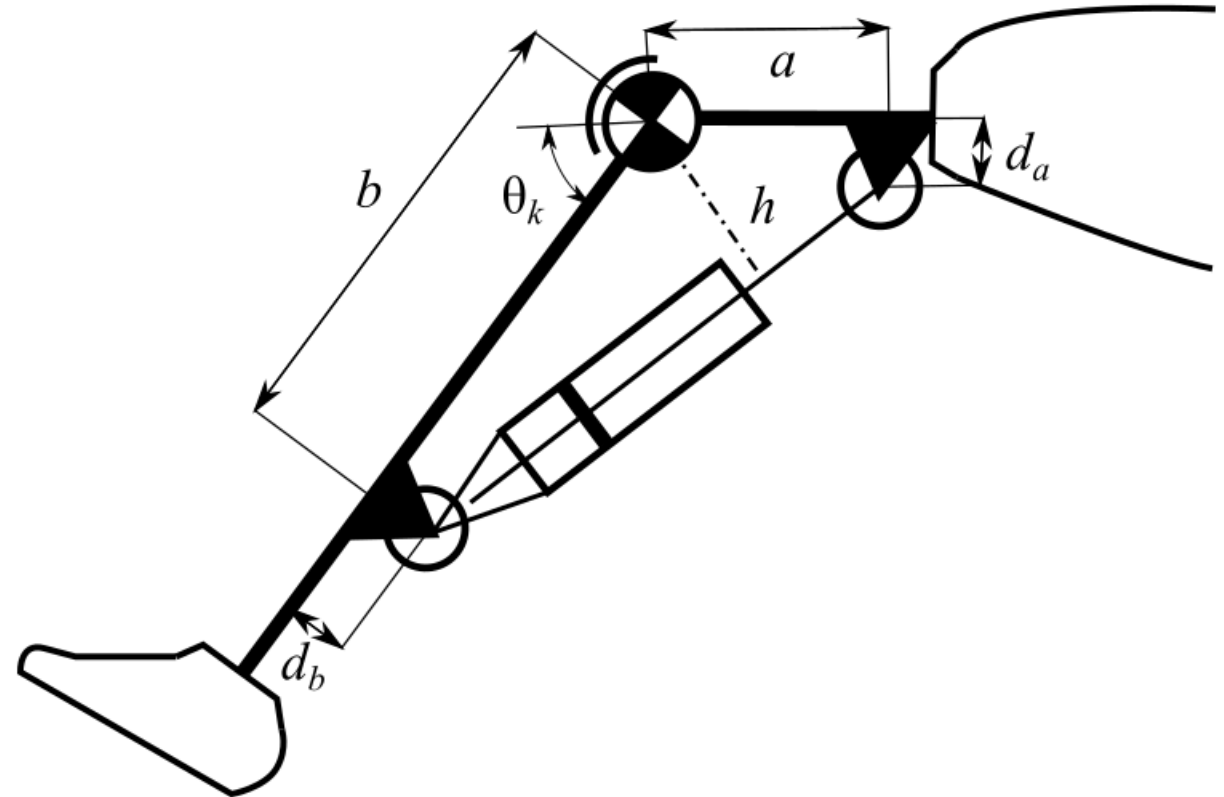
- ▶ Articular Actuation → Mimicking Muscle Working Principle
- ▶ Linear-Rotary Conversion:

$$\circ h(\theta_k, a, d_a, b, d_b) = \frac{T_k}{F} = \frac{v}{\omega_k}$$



Variable Transmission Ratio

- **Geometric** Parameters: a, d_a, b, d_b
 - Selected wrt geometric constraints
- **Physical** Quantity → Knee Angle θ_k



Development Process

- ▶ During the doctorate program, 2 prototypes have been developed:
 - **Test-rig Prototype**
 - Based on commercial-off-the-shelf (COTS) components
 - *Goal* → validate the linear EHA as a feasible actuator for knee prostheses without taking care of geometric and weight constraints
 - **Fully-integrated Prototype**
 - Based on fully custom designed components
 - *Goal* → enhance the actuator back-drivability and performance while satisfying the integration constraints in terms of size and weight



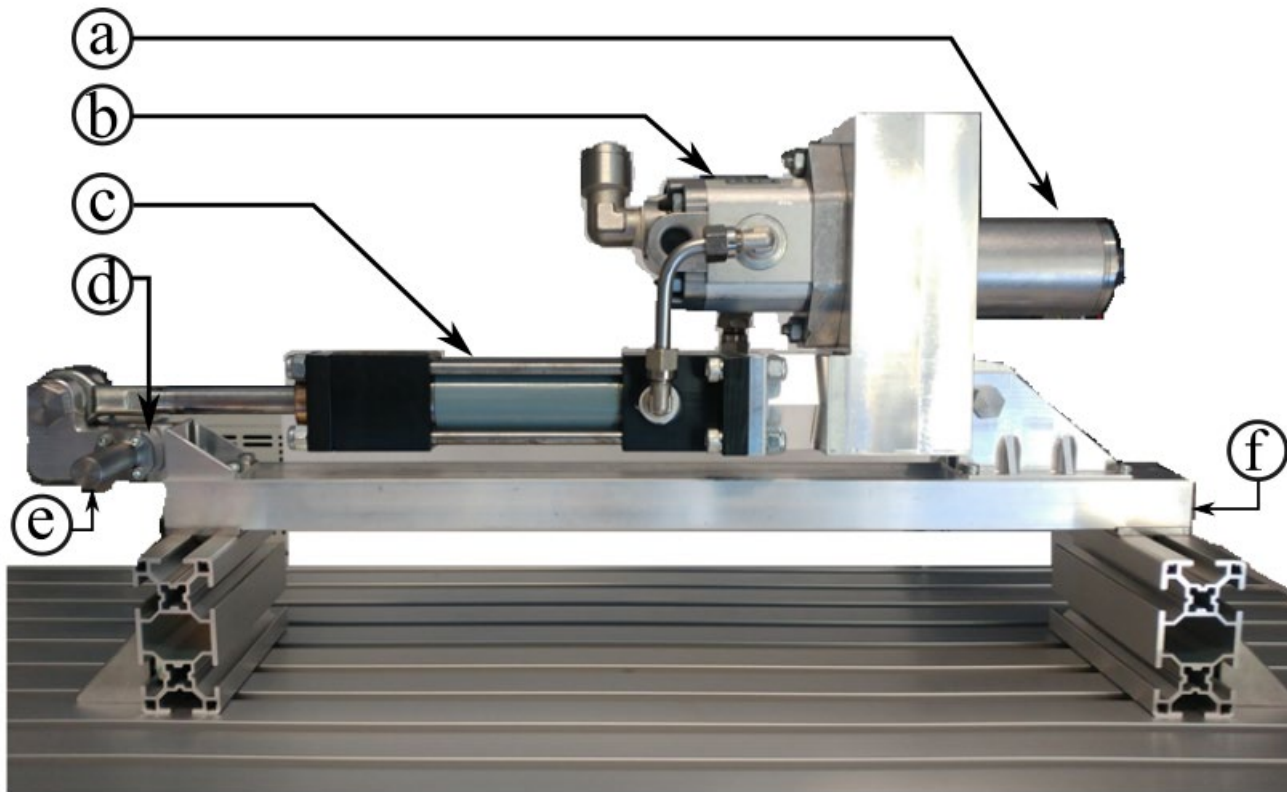
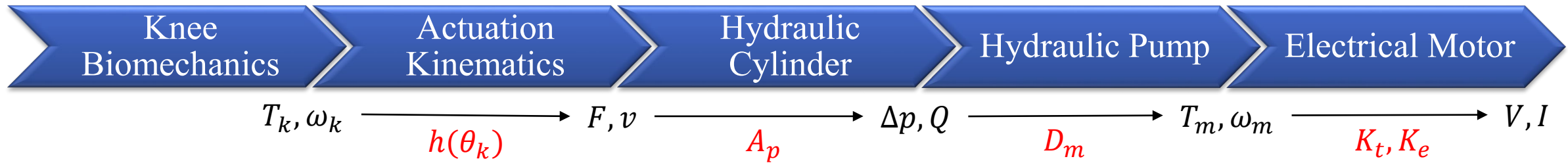
Test-rig EHA Prototype¹

➤ Design & Experimental Validation

Tessari, F., Galluzzi, R., Tonoli, A., Amati, N., Laffranchi, M., De Michieli, L., (October, 2020) "Analysis, Development and Evaluation of Electro-Hydrostatic Technology for Lower Limb Prostheses Applications" *IEEE Proceedings of International Conference on Intelligent Robots and Systems (IROS)* – ACCEPTED & UNDER PUBLICATION



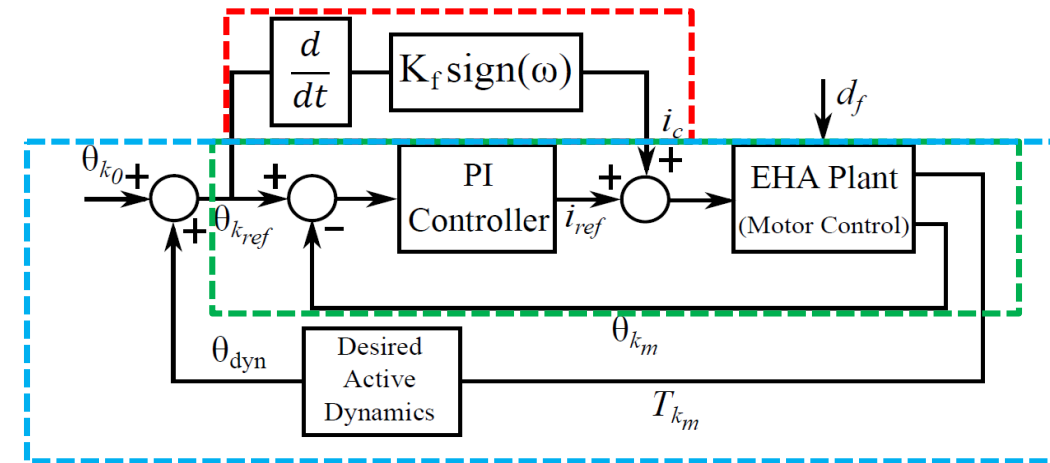
Assembled COTS I-EHA



- a) **Electrical Motor:** Maxon EC-i 40
- b) **Hydraulic Pump:** Bucher APR05/0.75
- c) **Hydraulic Cylinder:** FluidoSistem 25/12P
- d) Knee Joint
- e) Thigh-Connector
- f) Shin/Pylon

Implemented Control Strategy

- ▶ On the low-control level → A **current** control loop has been implemented on the electrical motor
- ▶ On the high-control level:
 - A **position tracking** control
 - Useful to assess the capability of the designed device
 - Required for the admittance control
 - An **admittance** control
 - Particularly suited for *natural walking and gait coordination enhancement*
 - Reduced number of control parameters
- ▶ Moreover → a **feed-forward friction compensation** to compensate for elevated hydraulic cylinder *friction, stick-slip and stiction* effects



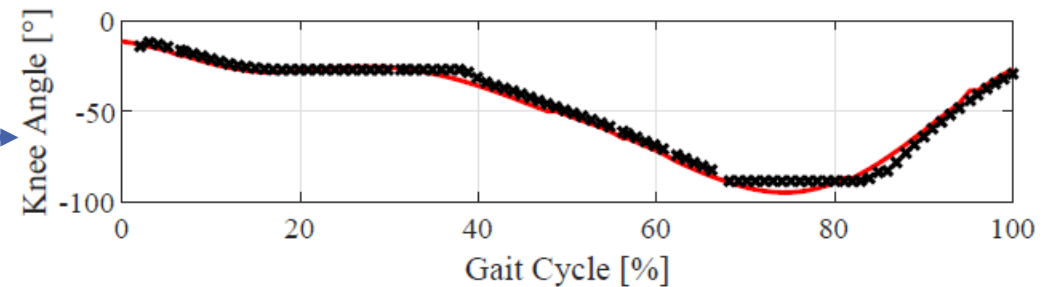
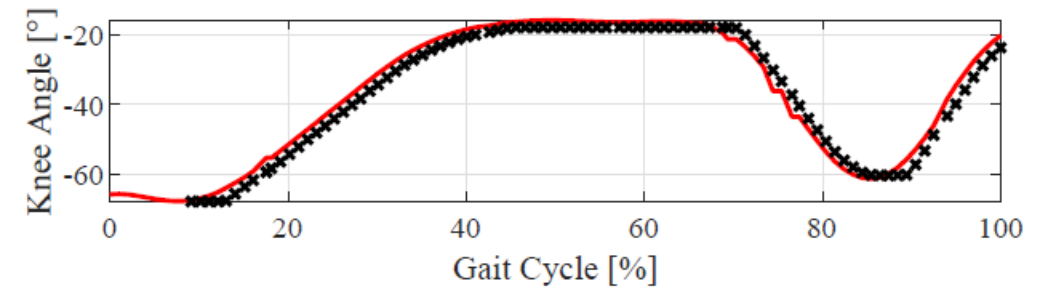
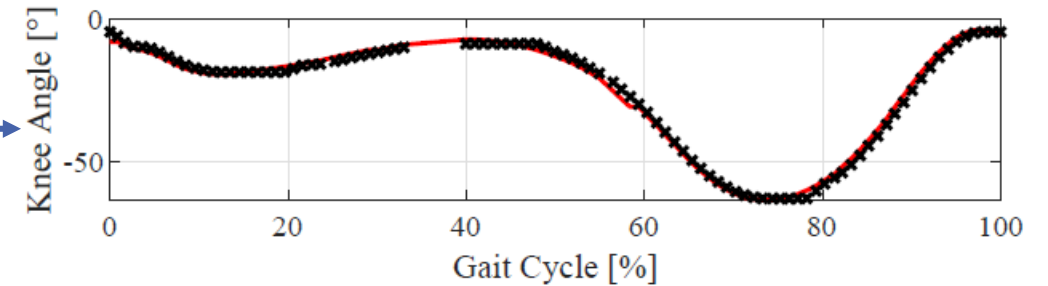
Position Tracking – Results

▶ 3 Different Gaits have been tested:

- Level Walking
- Stair Ascending
- Stair Descending

▶ Results shows **accurate** position tracking capabilities

- $1.5^\circ \leq |RMSE_{max}| \leq 3.4^\circ$



Admittance Control

- ▶ **Admittance Control** → Imposes a dynamic trajectory to the position control loop that is function of an *imposed mechanical behavior* (inertia, damping, stiffness)

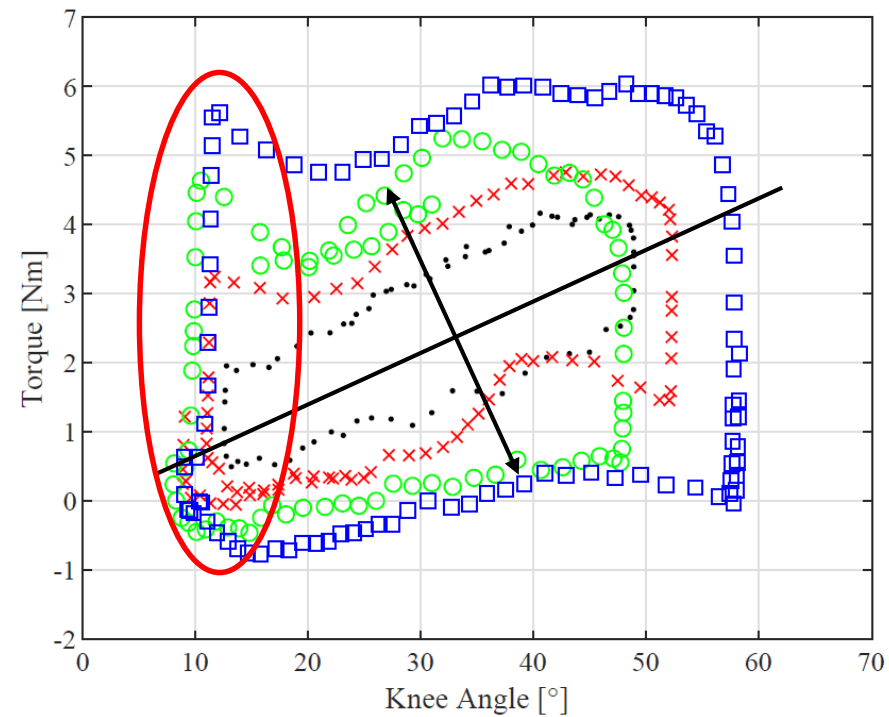
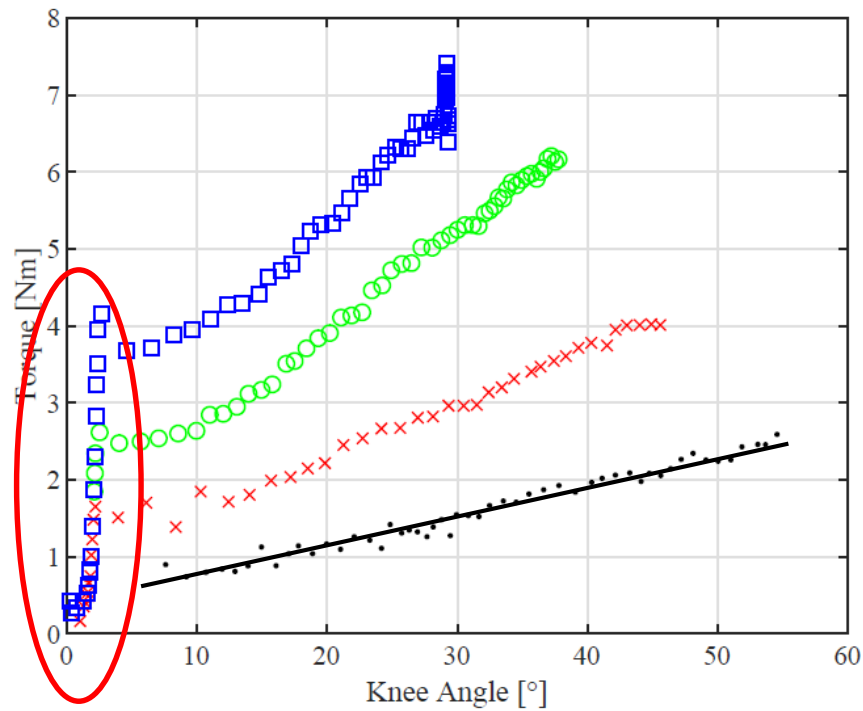
$$\theta_{k_{ref}} = \theta_{k_0} + \theta_{dyn}$$
$$\theta_{dyn} = \frac{T_{k_m}}{J_{k_{des}}s^2 + \beta_{k_{des}}s + k_{k_{des}}}$$

- ▶ In the specific case we focused on a **spring-damper dynamics** ($\beta_{k_{des}}, K_{k_{des}}$)

$$\theta_{dyn} = \frac{T_{k_m}}{\beta_{k_{des}}s + k_{k_{des}}}$$

Admittance Control – Results

- ▶ 2 Test campaigns →
 - $\beta = \text{const.} \wedge k = k_i, i = 1, \dots, n$
 - $k = \text{const.} \wedge \beta = \beta_i, i = 1, \dots, n$



Prototype Efficiency Mapping

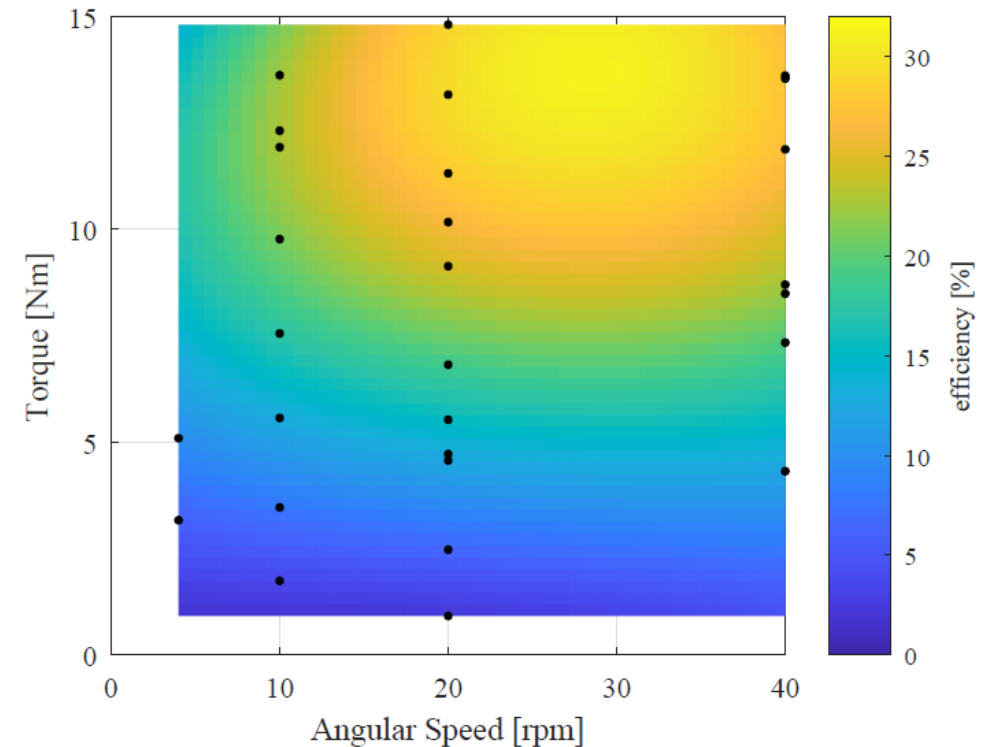
- ▶ An experimental efficiency map has been evaluated
 - Coupling the Prototype to a Dynamic Load

- ▶ The efficiency is calculated as:

$$\eta = \frac{P_{out}}{P_{in}} = \frac{T_k \cdot \omega_k}{V_{bus} \cdot I_{bus}}$$

- ▶ Results are compared to an electro-mechanical actuation with equivalent transmission-ratio
 - Comparison showed a **slightly higher** efficiency of EHA

- ▶ Unfortunately, the **frictions** were too high to operate the developed EHA as brake/damper → impossible energy harvesting



Fully-integrated EHA Prototype²

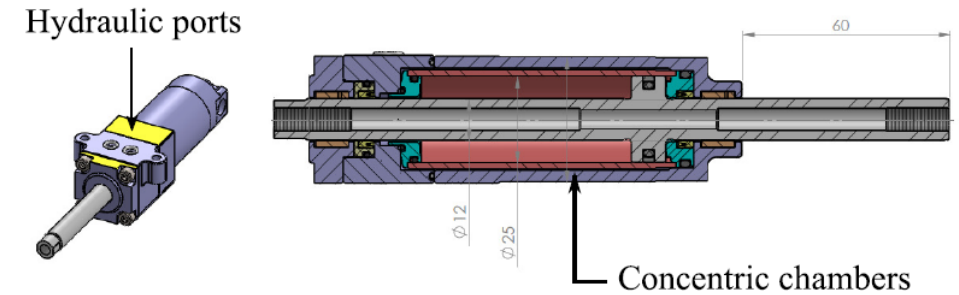
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- Tessari, F., Galluzzi, R., Tonoli, A., Amati, N., Milandri, G., Laffranchi, M., De Michieli, L., (December, 2020) “An Integrated, Back-Drivable Electro-Hydrostatic Actuator for a Knee Prosthesis” *IEEE Proceedings of International Conference on Biomedical Robotics and Biomechatronics (BioRob)* – ACCEPTED & UNDER PUBLICATION



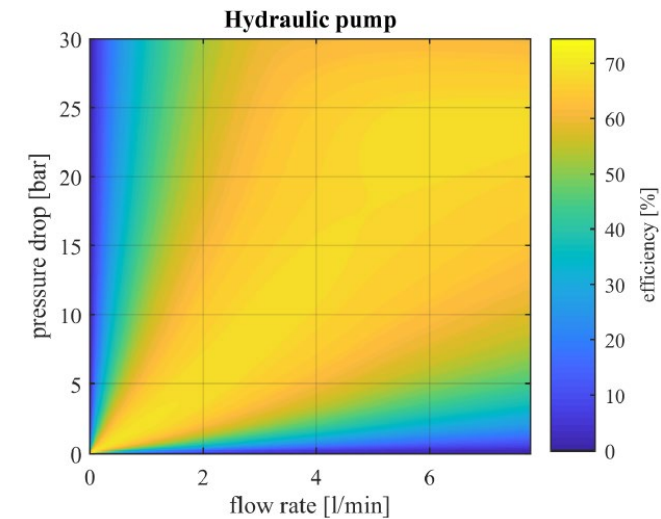
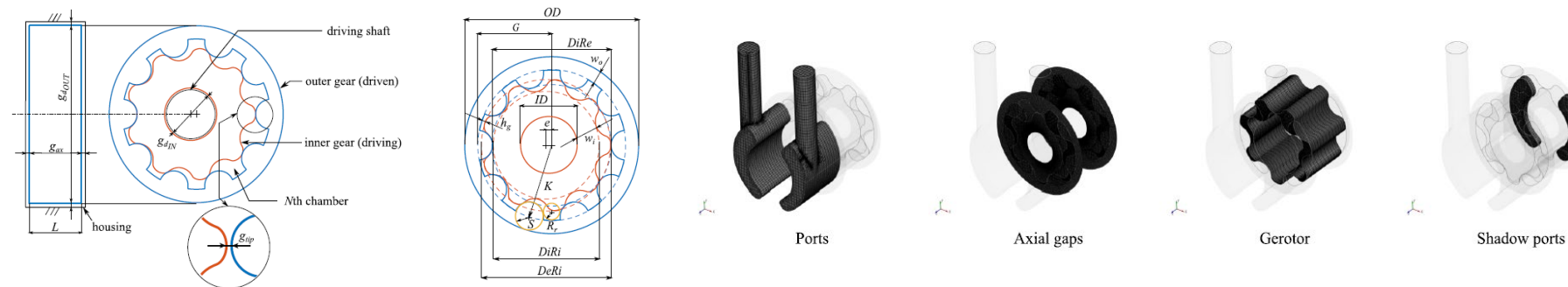
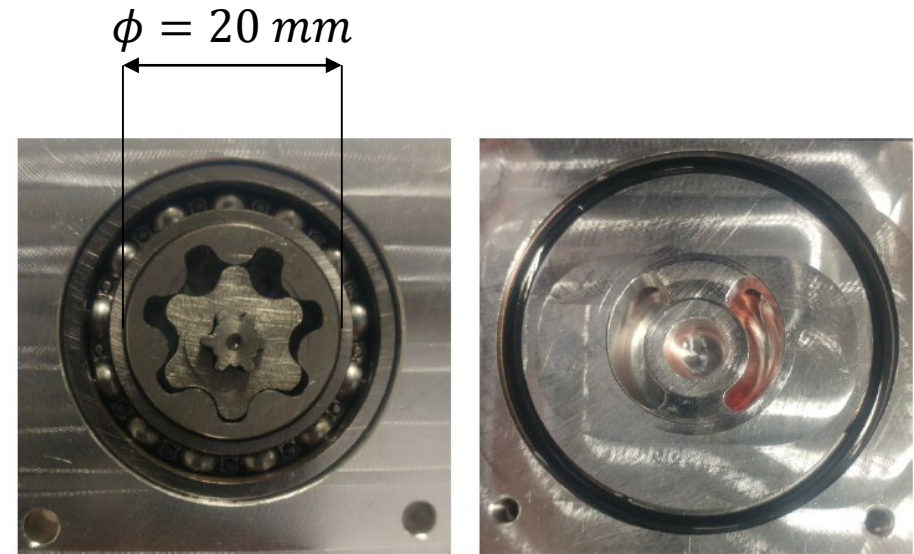
Hydraulic Cylinder – Design

- ▶ Architecture → passing-shaft
 - No need of accumulators
- ▶ Same A_p , D , d were maintained
- ▶ Design Upgrades
 - To enhance **integration**:
 - Concentric chambers → Reduced radial size
 - Adjacent hydraulic ports → Minimized hydraulic circuitry
 - To enhance **performance**:
 - Utilization of high-performance PTFE seals → Reduced frictional effects



Hydraulic Pump – Design

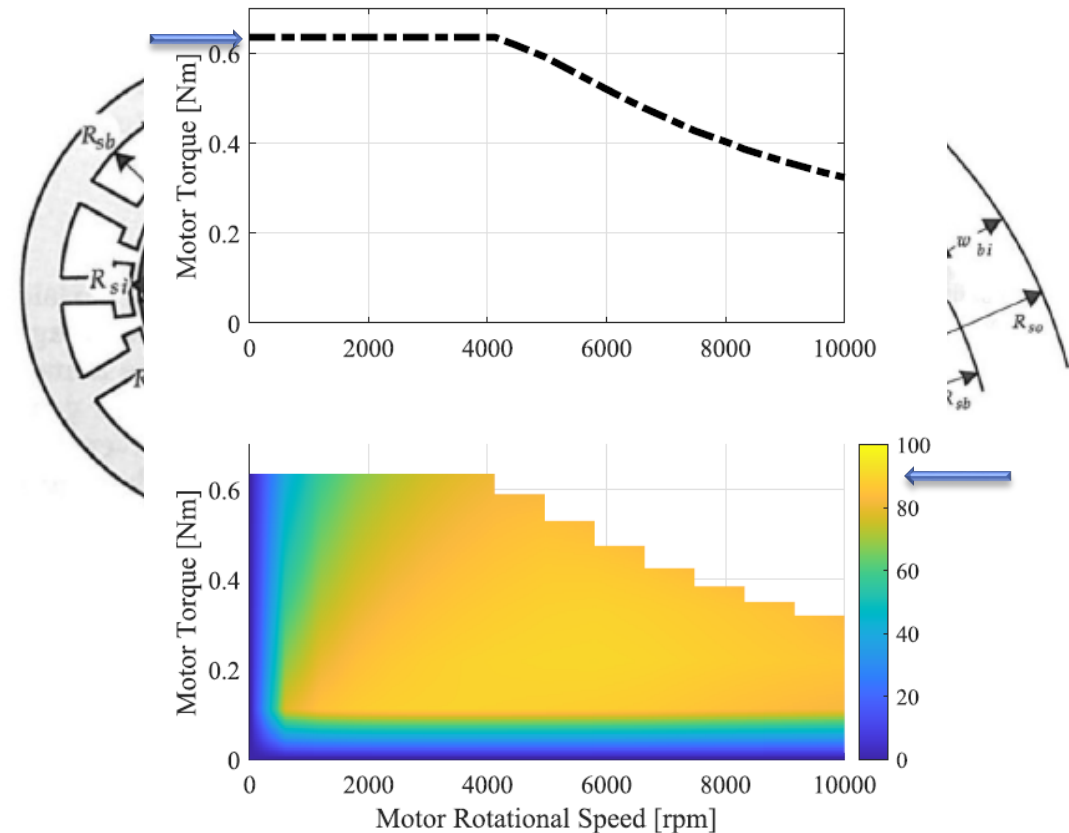
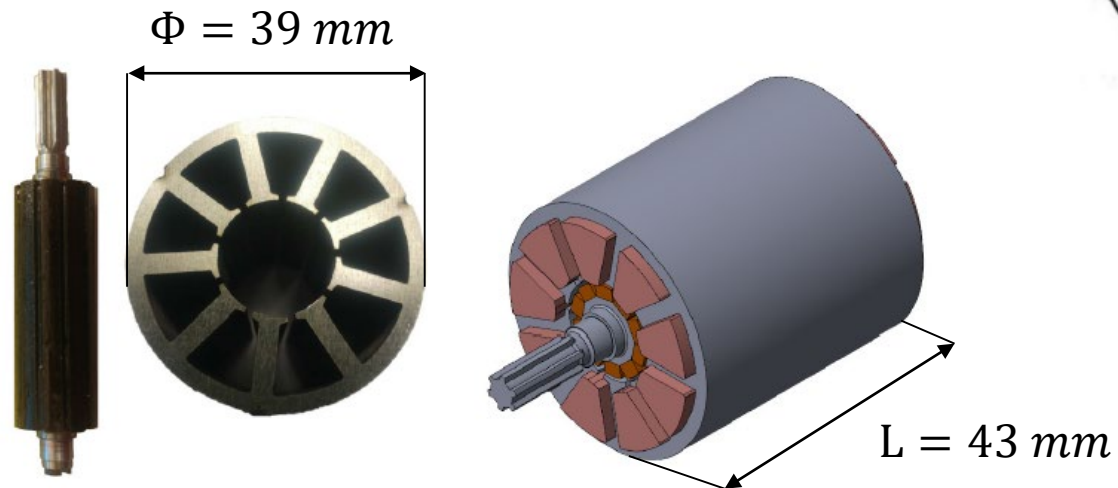
- ▶ Same Volumetric Displacement $\rightarrow D_m = 0.75 \frac{cc}{rev}$
- ▶ Pump Architecture \rightarrow Custom **Gerotor** Pump
 - **Lower noise** compared to external gear pump
 - **More compact** compared to external gear pump
- ▶ Dedicated design methodology to enhance¹:
 - Volumetric Efficiency



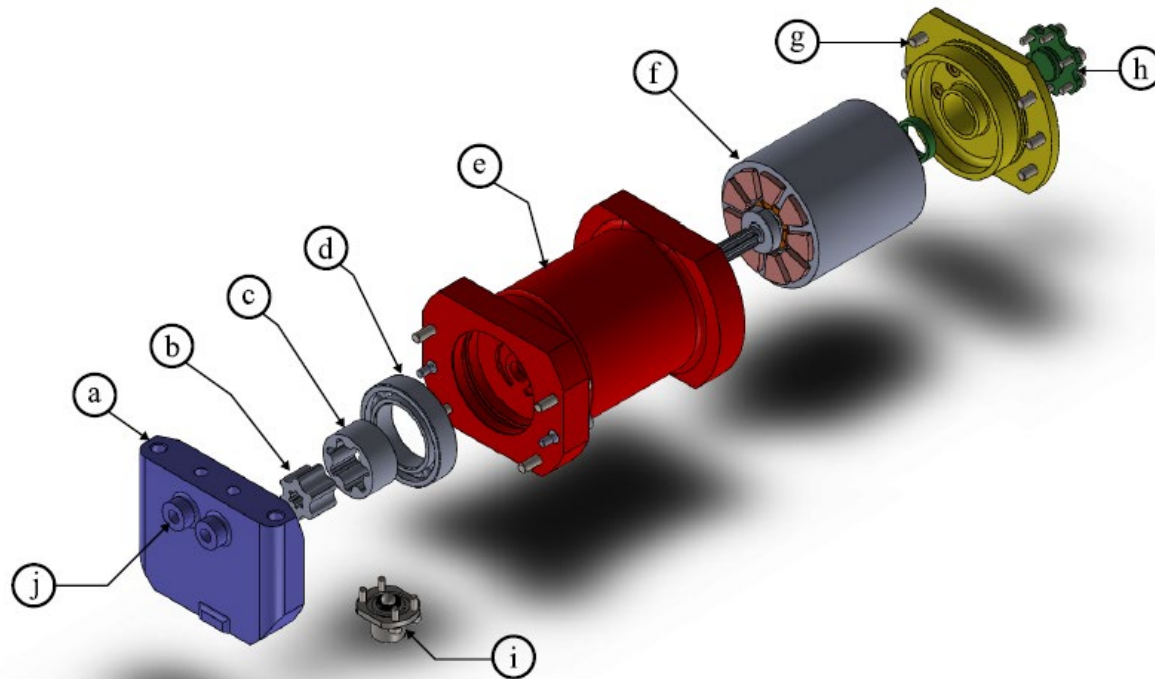
Tessari, F., Galluzzi, R., and Amati, N. (November 6, 2019). "Efficiency-Driven Design Methodology of Gerotor Hydraulic Units." *ASME. J. Mech. Des.* doi: <https://doi.org/10.1115/1.4045421>

Electrical Motor – Design

- ▶ Design a custom PMSM capable of satisfying the Knee Requirements
- ▶ Motor design methodology:
 1. Analytical modelling (Matlab)
 2. Magnetic optimization (Comsol)
 3. Electrical simulation (FluxMotor)



Assembled Fully-Integrated I-EHA

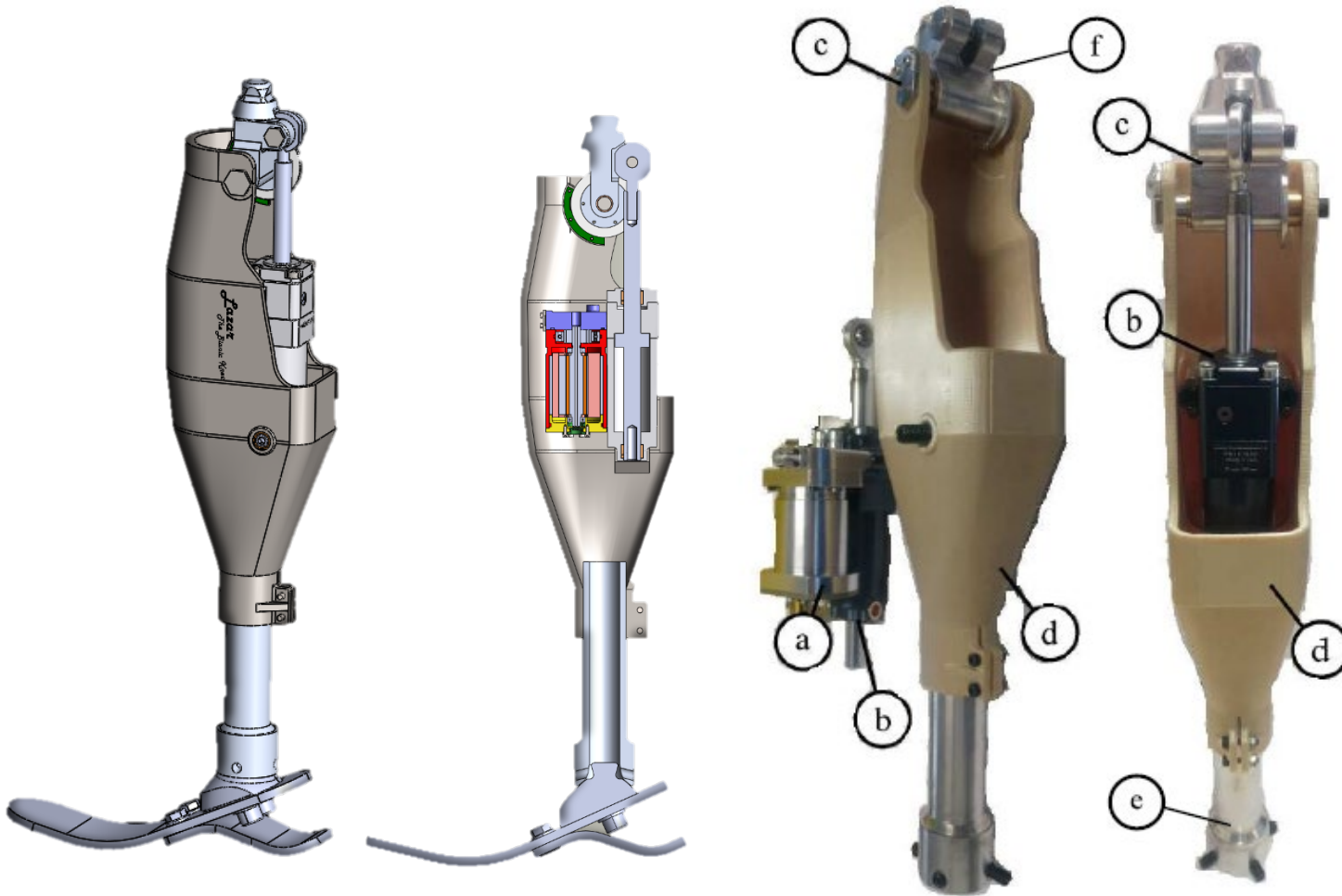


$$V = 123.5 \times 91 \times 60 \text{mm}^3$$

$$M = 1.2 \text{ kg}$$

- a) Pump cover.
- b) Inner gear.
- c) Outer gear.
- d) Pump ball bearing.
- e) Case.
- f) Electrical Motor.
- g) Anodized Actuator Plug.
- h) Motor Hall Sensors Housing.
- i) Pre-loading valve.
- j) Pressure sensors ports.

Assembled Fully-Integrated Prosthetic Knee



- a) Motor-Pump Group
- b) Hydraulic Actuator
- c) Knee Joint
- d) Actuator Chassis
- e) Pylon connector
- f) Thigh connector

Designed to reach:

$$T_{max} \approx 45 \text{ Nm}$$

$$\omega_{max} \approx 60 \text{ rpm}$$

(to satisfy level walking requirements)

Position Tracking – Results

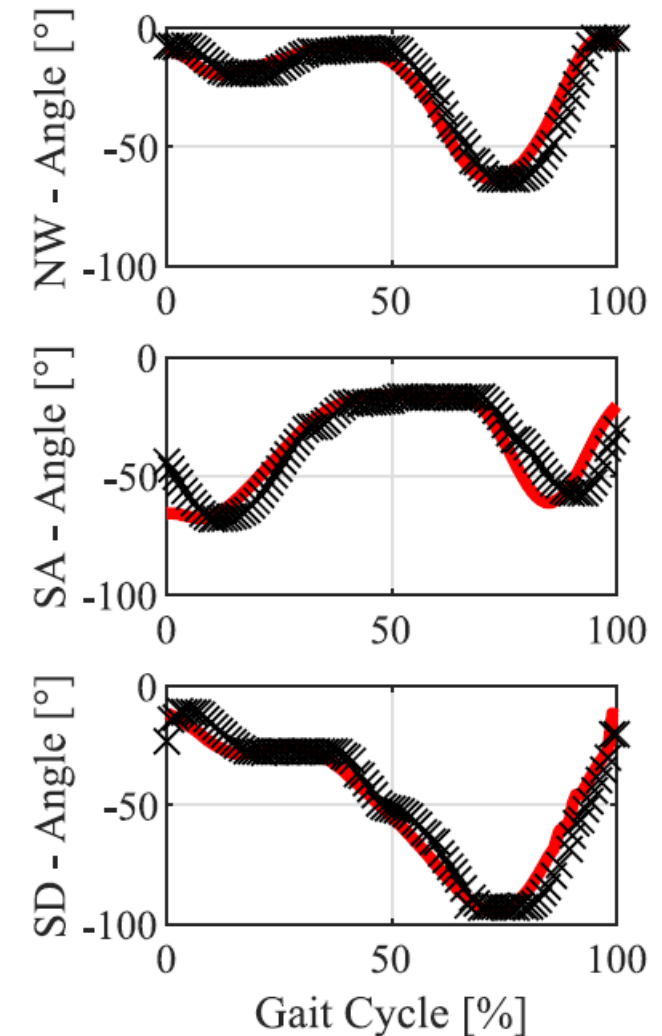
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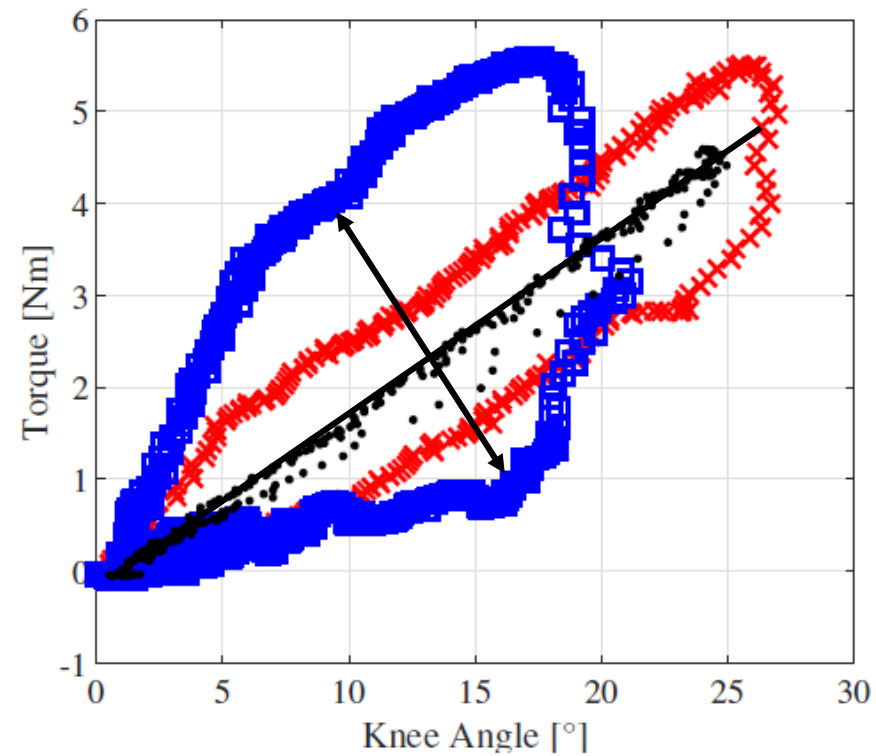
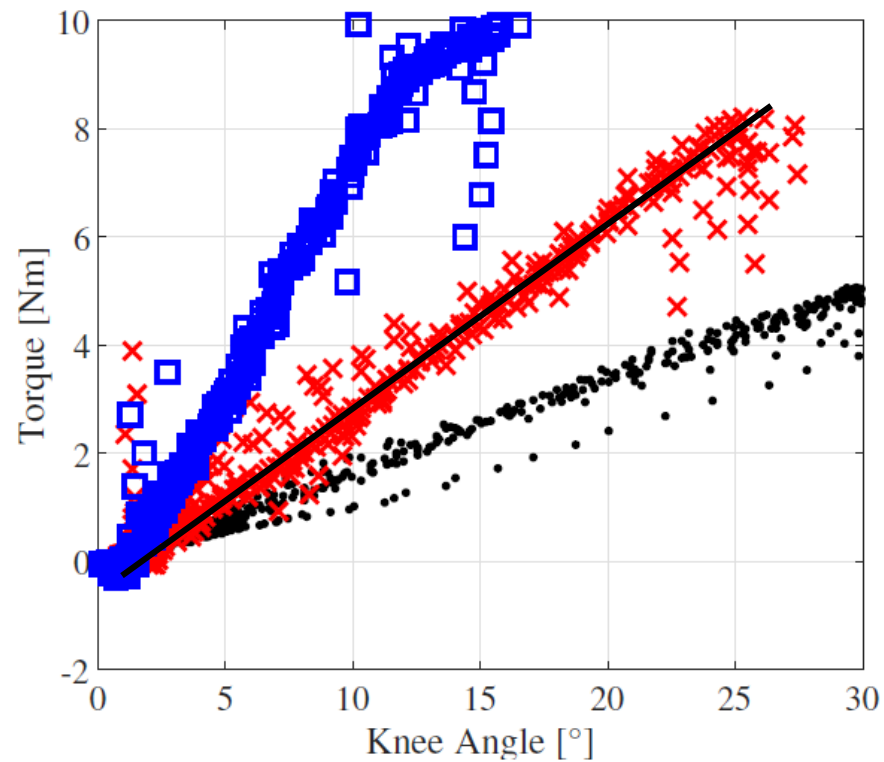
- $5.5^\circ \leq |RMSE_{max}| \leq 7.4^\circ$

Worse with respect to first prototype → due to leakage in the hydraulic unit



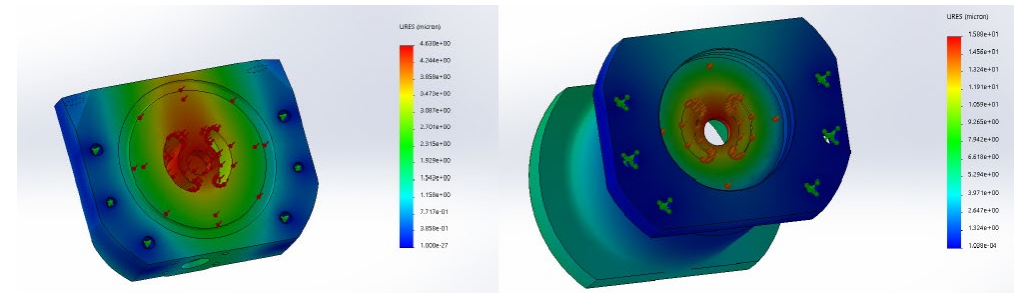
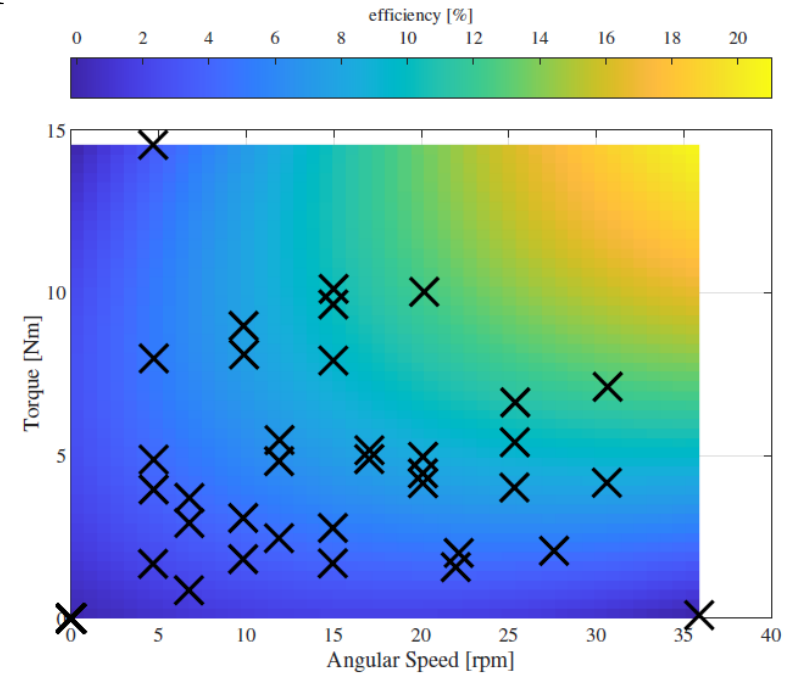
Admittance Control – Results

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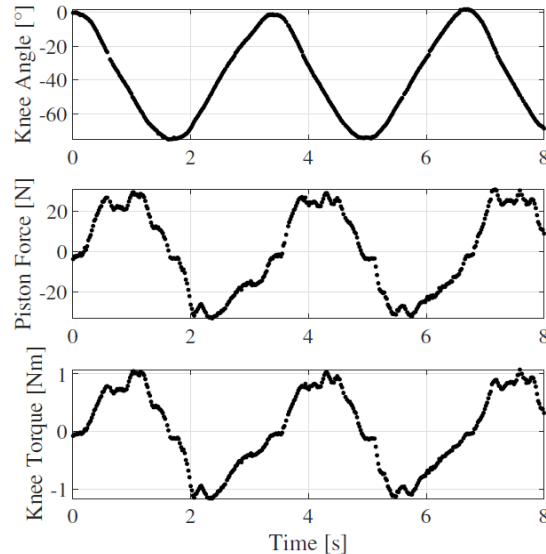
Efficiency Mapping

- ▶ Similarly to the test-rig EHA, the efficiency map as an actuator has been experimentally computed
- ▶ A worsening of the performance is observable
 - Peak efficiency @ (15 Nm, 35 rpm) dropped:
 - η : 30% \rightarrow 21%
- ▶ Source of the performance loss:
 - Un-modeled deformation of the pump housing
 - leading to an almost *doubled pump axial clearance*
 - *Breaking down volumetric efficiency* of the pump



Regenerative Braking

- ▶ The fully-integrated EHA demonstrated to be **highly back-drivable**
 - $T_{bd} \leq 1 \text{ Nm} @ \omega_k = 7.5 \text{ rpm}$

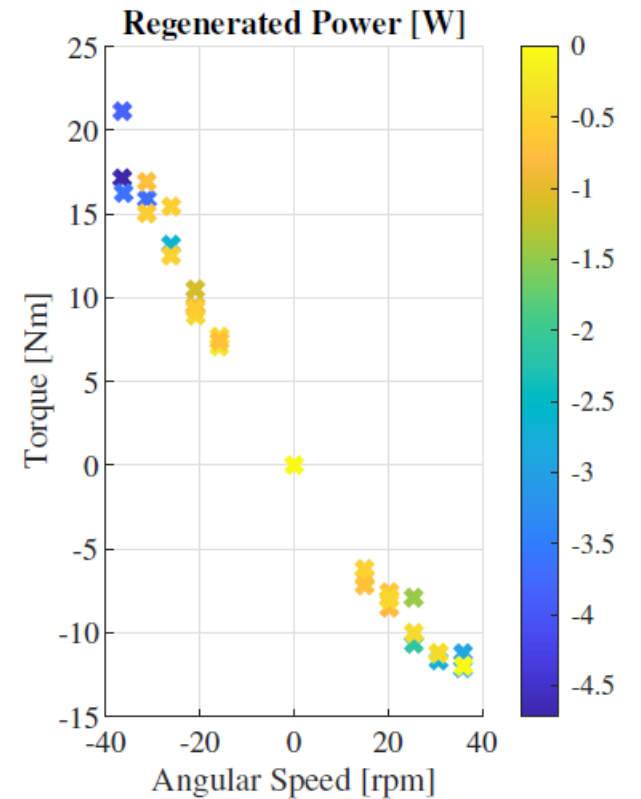
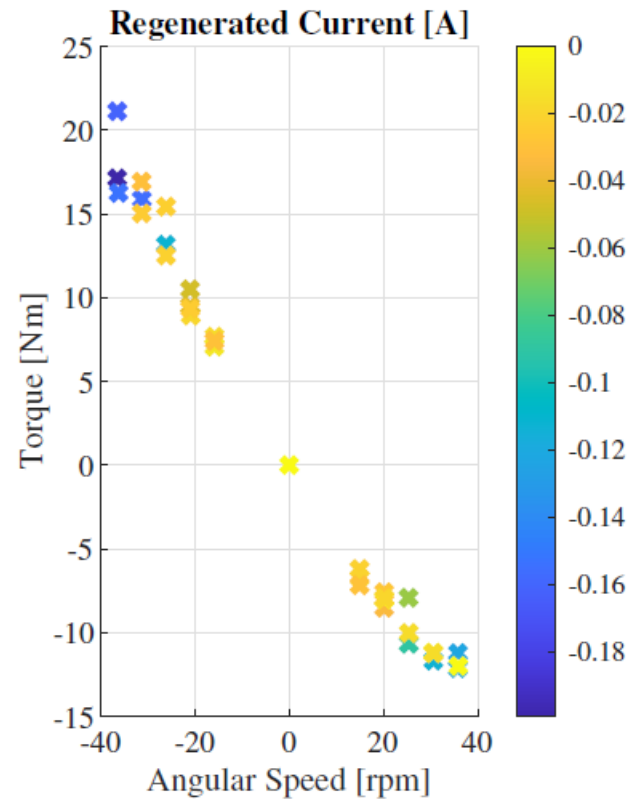
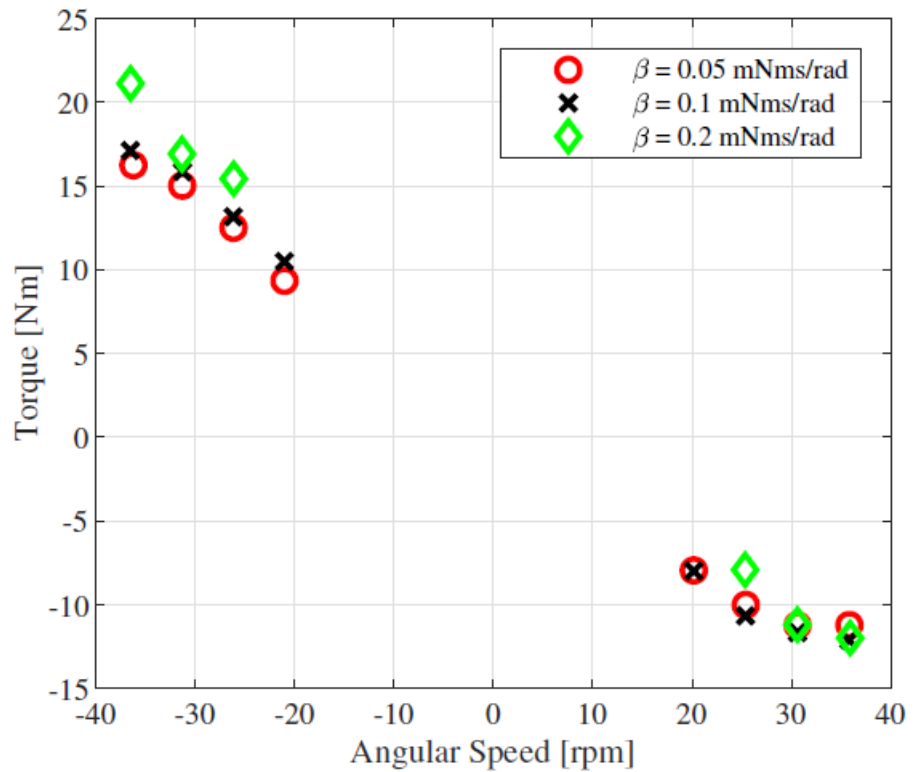


- ▶ As a consequence, regenerative braking control technique have been implemented
 - It consists on imposing a current proportional to the rotating speed of the motor and opposite in sign

$$i_{ref} = -\frac{1}{K_T} \beta_{reg} \omega_{m_m}$$

Regenerative Braking – Results

- ▶ Different damping coefficients β_{reg} have been tested \rightarrow for each of them the regenerated current I_{reg} and power P_{reg} have been computed

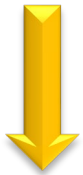


Conclusions

Intermediate Solution



- Medium functionality
- Light-medium weight
- Optimized Energy Consumption

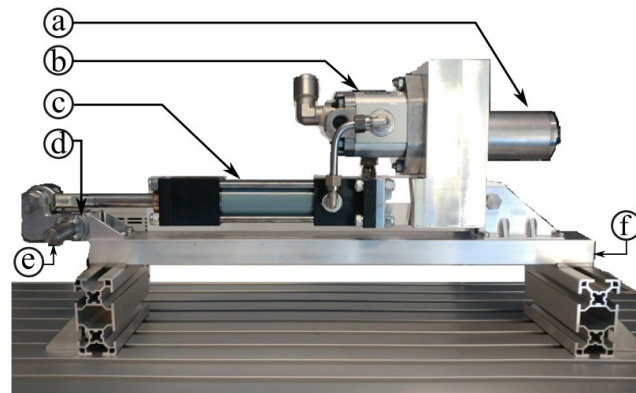


- **Efficiency**
 - Comparable/Better Perf.
- **Integration**
 - Compact & Light-weight
- **Back-drivability**
 - Controllability & Reg. Braking

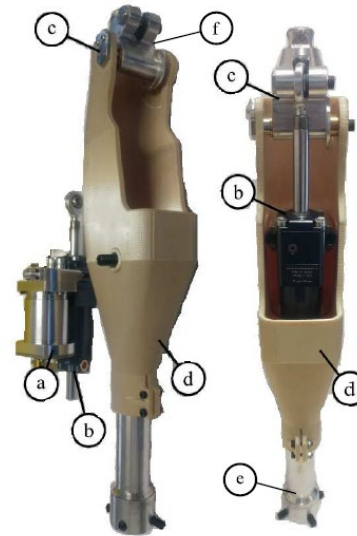
- ▶ The resulting **EHA prototypes** demonstrated to be able to satisfy the starting goals.

Specifically:

• 1st Prototype



• 2nd Prototype



Future Developments

- ▶ An **upgraded version** of the fully-integrated EHA is **under development** on the basis of the presented results
- ▶ The developed actuator will be tested in the next months in the **real-case scenario** on a sensorized tread-mill to investigate its capabilities also in the field of application
- ▶ “Human” level control strategies are under investigation to guarantee a better **human-machine interaction**



Thanks for your attention!



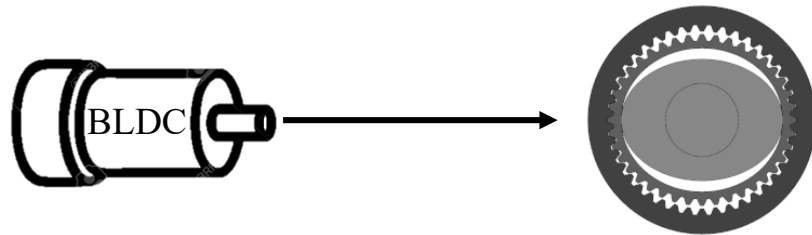
Back-Up Slides

➤ Support Material

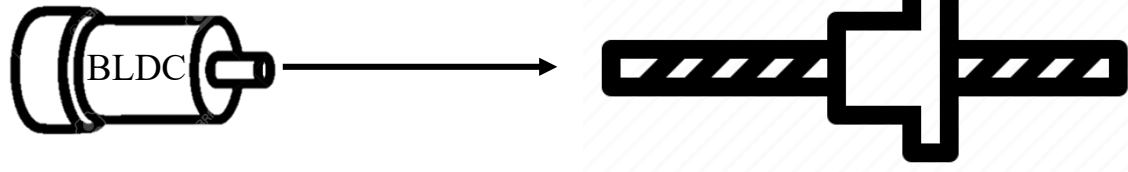


Active Prostheses – State-of-the-art


- ▶ The analysis of the state-of-the-art of active knee prostheses – both commercial products and research prototypes – shows a particular focus on:
 - **Electro-mechanical actuation**
 - Specifically two main trends can be observed



- Screw-Based



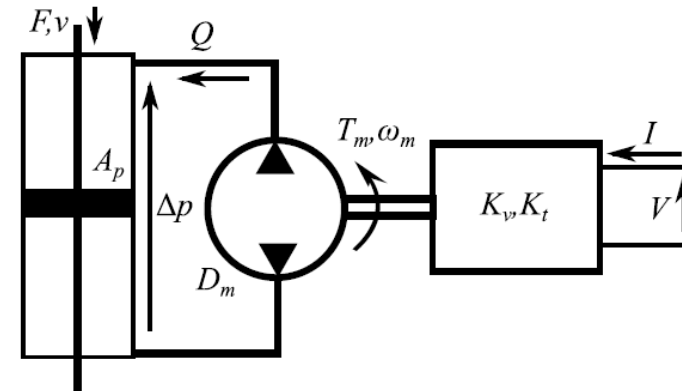
Active Prostheses – State-of-the-art

- ▶ The analysis of the state-of-the-art of active knee prostheses – both commercial products and research prototypes – shows a particular focus on:
 - **Electro-mechanical actuation** → **Gear-based & Screw-Based** 
- ▶ The resulting devices are often **bulky, non-integrated** and **poorly efficient**
- ▶ The design is mainly focused on reaching Torque-Speed requirements without considering:
 - **Integration** → the prosthesis must be *light-weight* while contained within the *anthropometric geometrical constraints* of a physiological lower leg
 - **Back-drivability** → a back-drivable prosthesis would guarantee a much better *human-machine interaction*, as well as, control of the device
 - **Efficiency** → a higher efficiency will lead to *lower energetic consumption* of the prosthesis, and thus a *longer autonomy* of the system

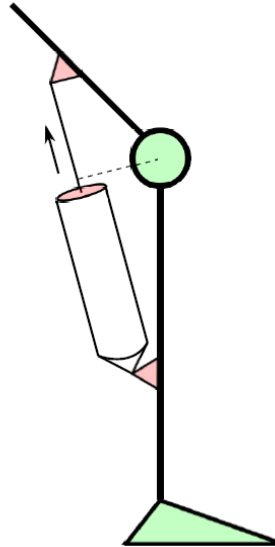
Design Approach

▶ **Linear** EHA has been chosen due to **2** main advantages:

- Better Mass Distribution
- Variable (Angle-Dependent) Transmission Ratio



Linear Actuation

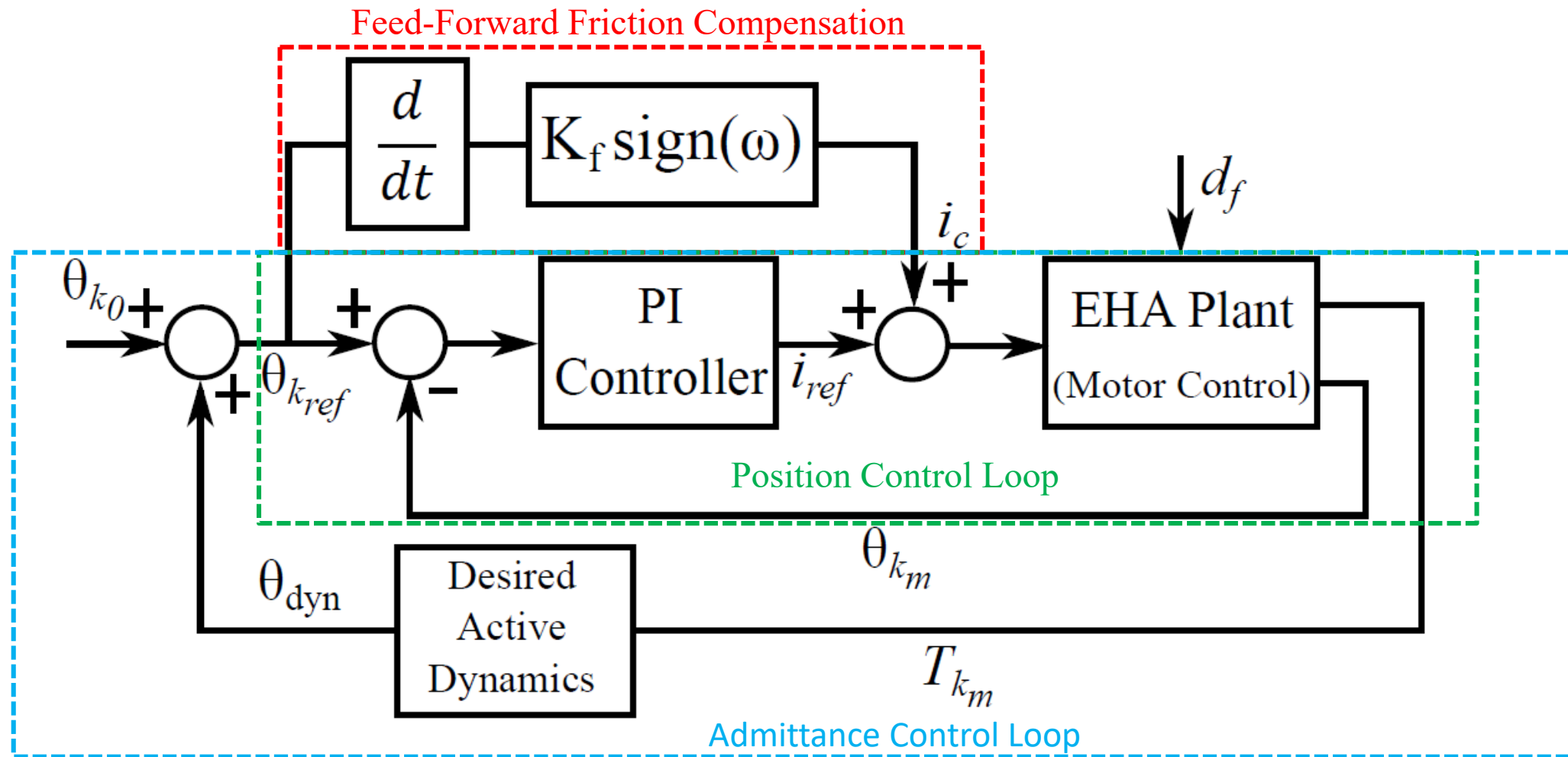


▶ **Top-Down** Design Strategy →

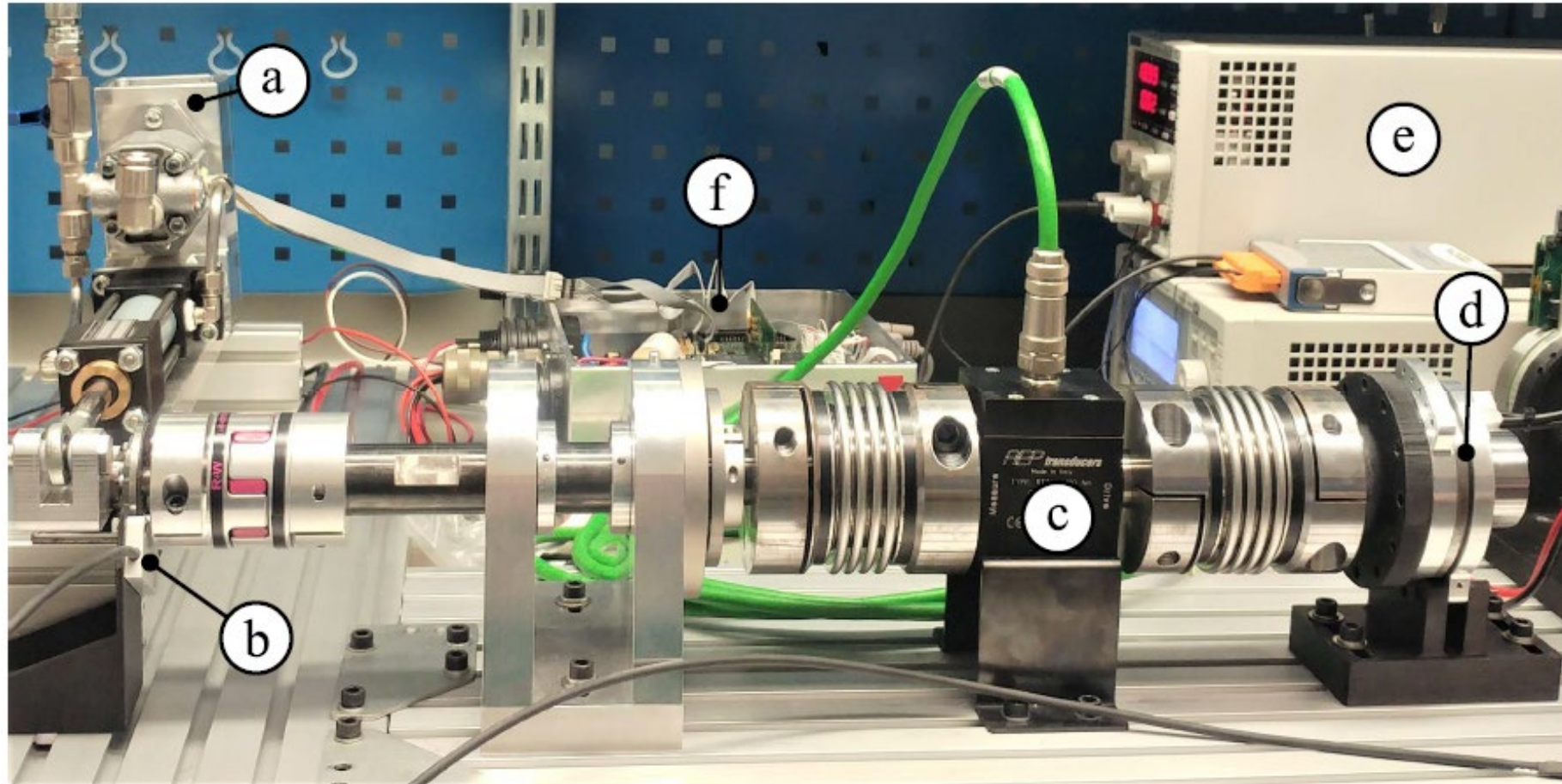
from Biomechanical Knee Requirements to Sub-component Specifications



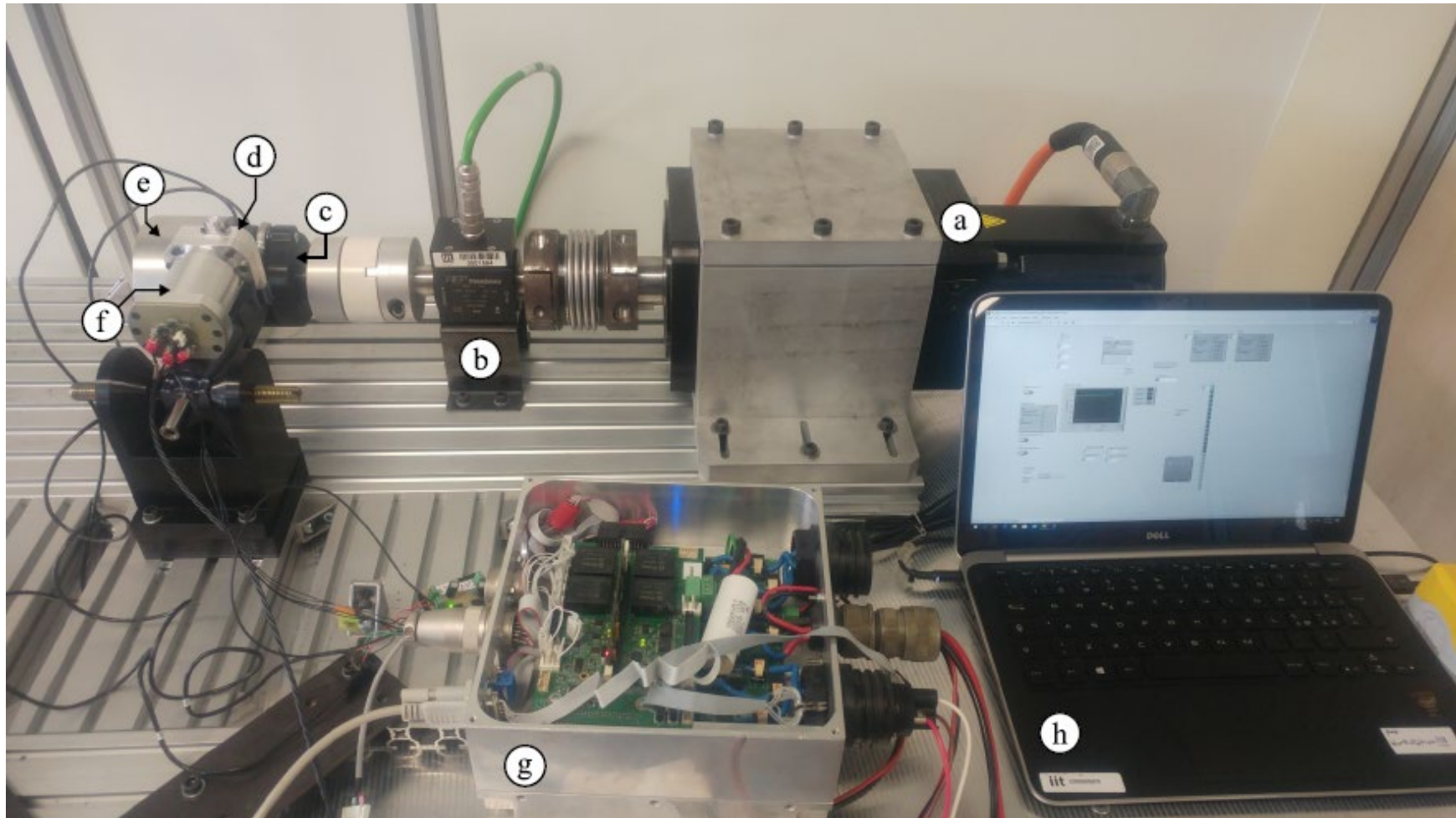
Control Strategy Block Scheme



Test Bench



Test Bench

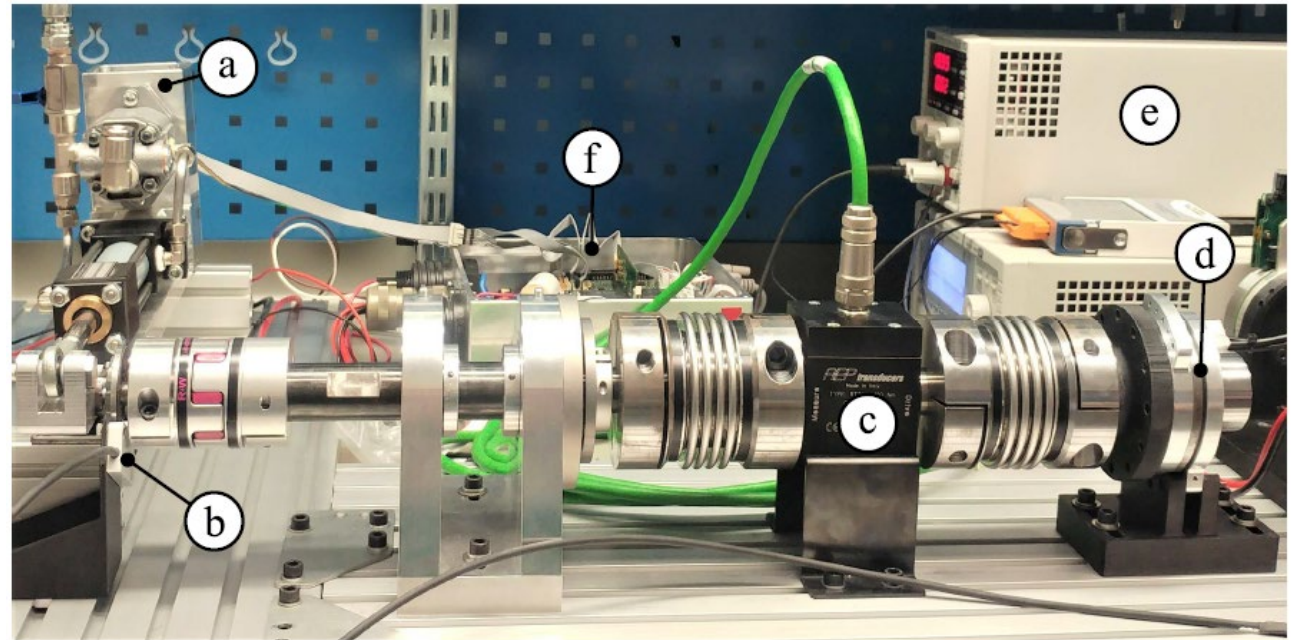


Test Bench & Sensors

- ▶ To implement the different control strategies
 - Digital Hall Sensors → for the Electrical Motor Control
 - Analogue Encoder → for the Knee Angular Position Control
 - Torque Transducer → for the Knee Force-based Control

- ▶ Resulting Test Bench

- a) EHA Prototype
- b) Knee Encoder
- c) Torque Transducer
- d) Load Drive
- e) Power Supply
- f) Control and Power Stage

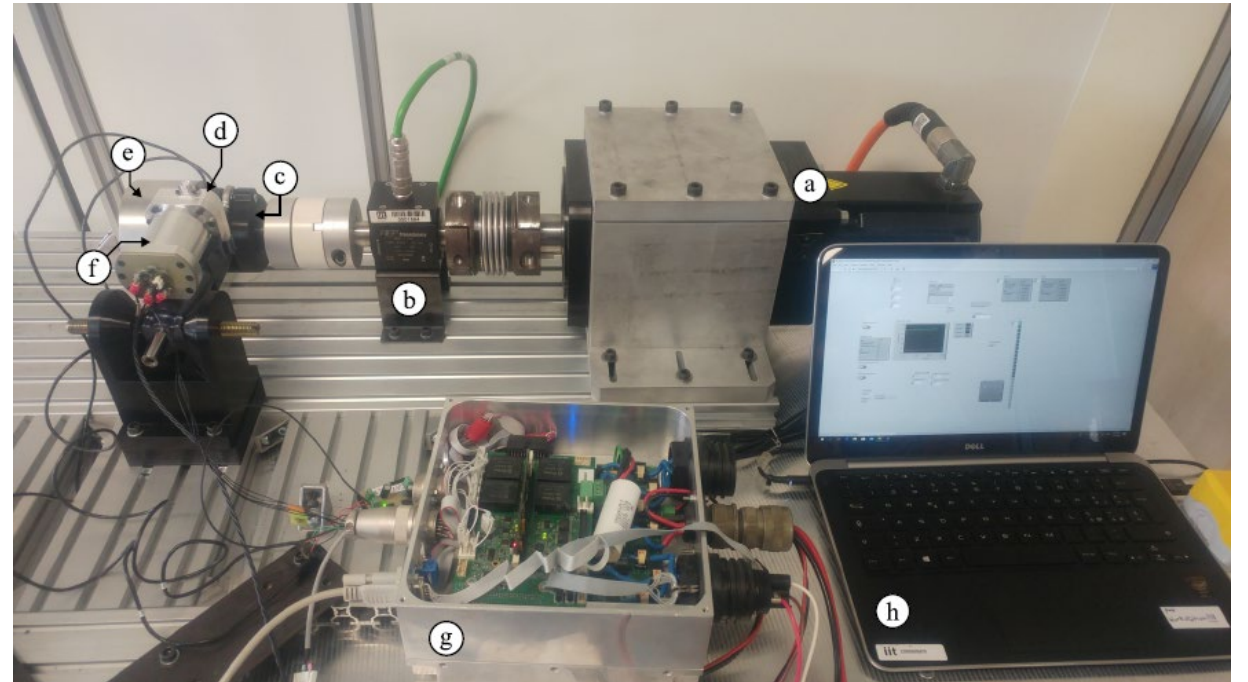


Test Bench

- ▶ To implement the different control strategies
 - Analogue Hall Sensors → for the Electrical Motor Control
 - Analogue Encoder → for the Knee Angular Position Control
 - Torque Transducer → for the Knee Force-based Control

- ▶ Resulting Test Bench

- a) Load Drive
- b) Torque Transducer
- c) Knee Joint
- d) Pressure gauges
- e) Knee Encoder
- f) Fully-integrated EHA
- g) Control & Power Stage
- h) Test bench computer main controller



Conclusions

- ▶ The doctorate path led to the design of 2 electro-hydrostatic actuators:
 - The **test-rig prototype**
 - Demonstrated to represent a valid substitute to classical electro-mechanical actuation showing *comparable efficiency* performance, while showing *good controllability*
 - On the other hand, the lack of components integration and optimization, led to a bulky and non-backdrivable device
 - The **fully-integrated prototype**
 - Showed that a dedicated process of components customization and integration, actually guarantees a much more *integrated, light-weight* and *back-drivable* device. The developed actuator is highly controllable and its back-drivability allows *energy harvesting* during gait.
 - Some limitations have been found in the *pump housing design*, which broke down the efficiency performance. However, a set of possible solutions is already under analysis to compensate it.

