



Corso di Dottorato in Ingegneria Meccanica

Ciclo XXX

Hydrodynamics Modelling and Mooring design of floating Wave Energy Converters

Tutor:

Prof.ssa Giuliana Mattiazzo



Offshore

Renewable

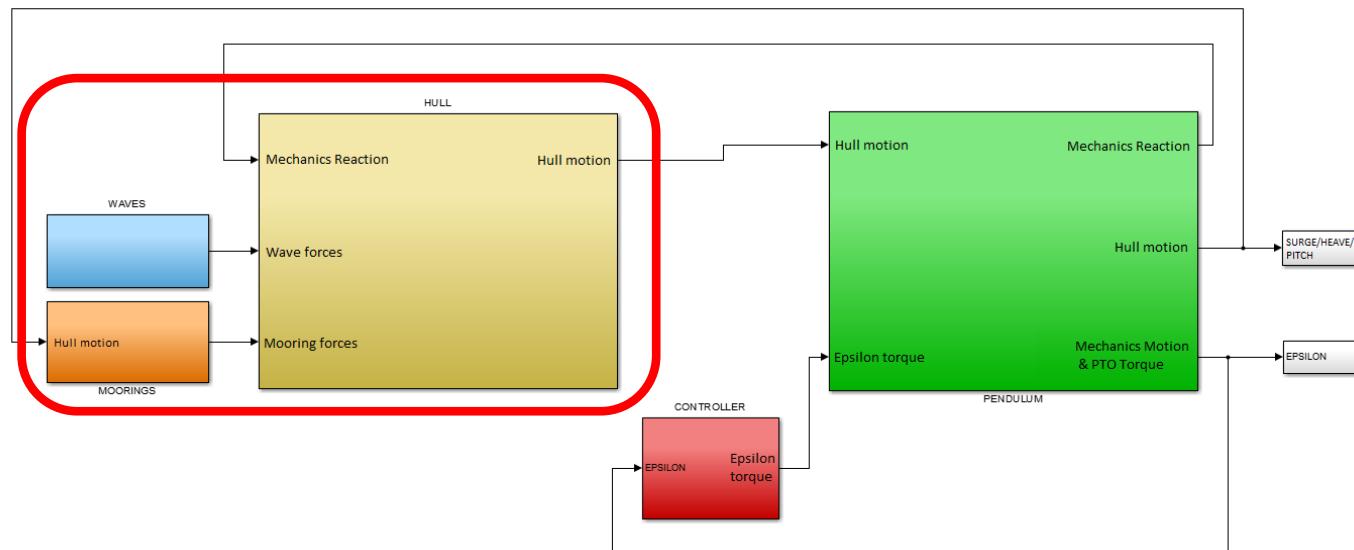
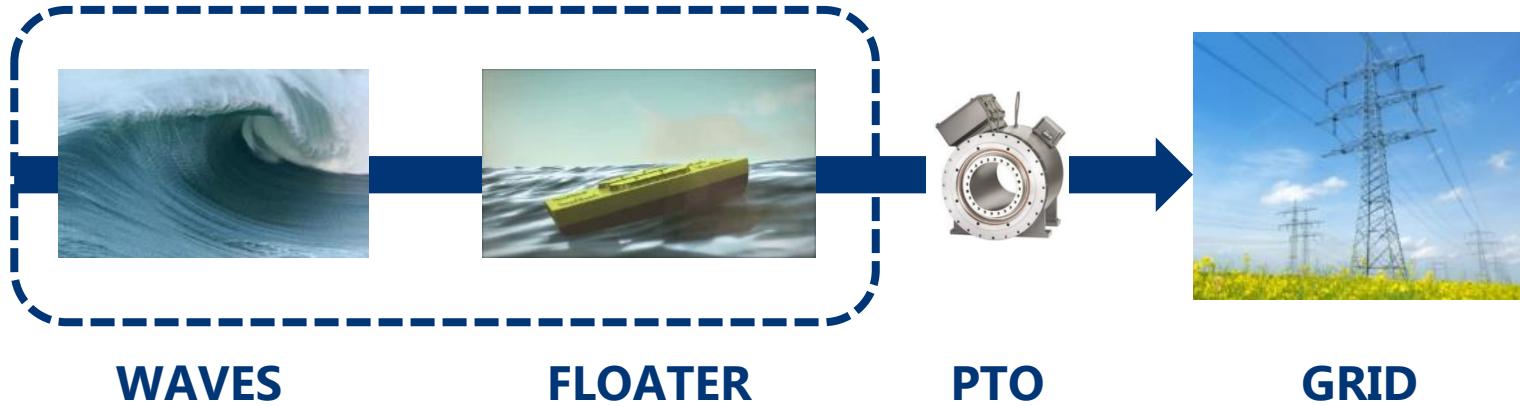
Energy

Candidate:

Biagio Passione

biagio.passione@polito.it

Design Tool – Simulink Wave to Wire model



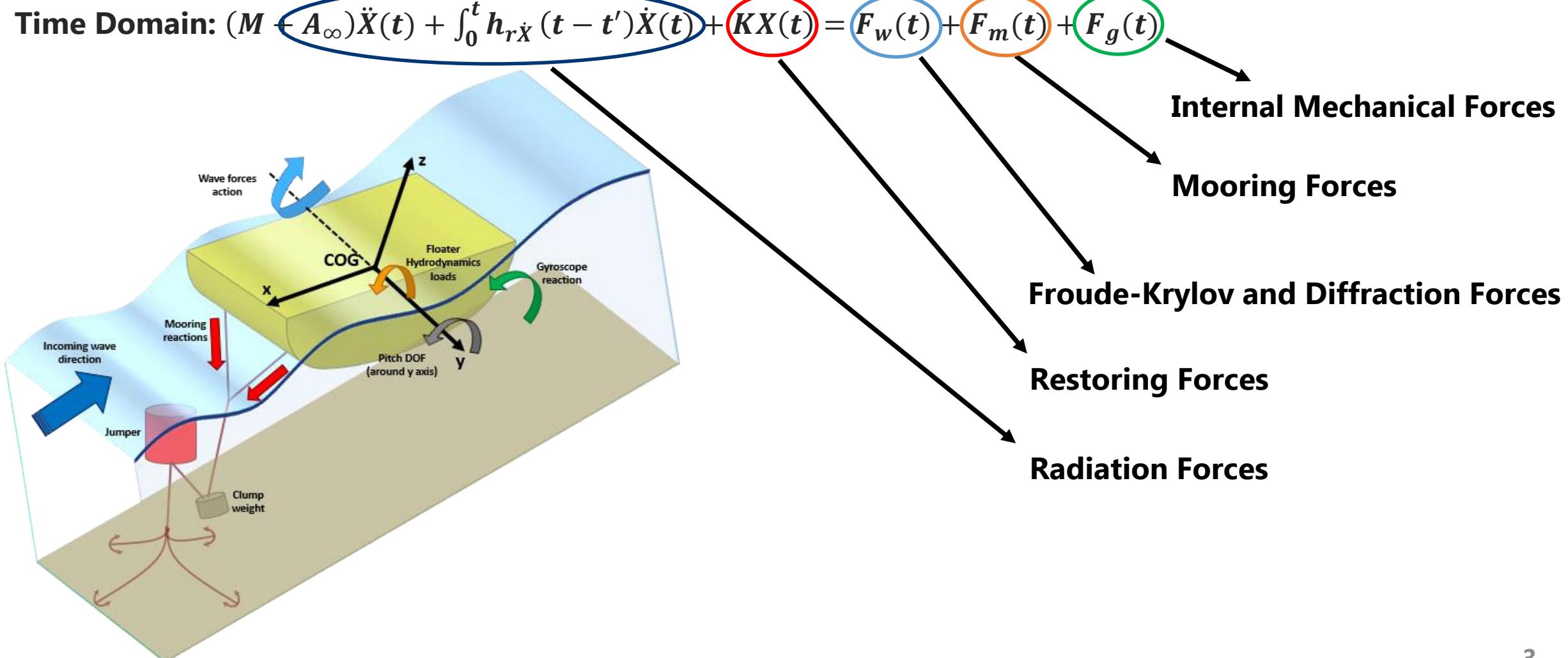
Motivation

- Numerical model improvement
- Analysis of non-linear effects
- Mooring design
- Mooring influence on dynamics

Hydrodynamic interactions – Potential flow

Mathematical model – Cummins' equation

Time Domain: $(M + A_{\infty})\ddot{X}(t) + \int_0^t h_r \dot{X}(t-t') \dot{X}(t) + KX(t) = F_w(t) + F_m(t) + F_g(t)$



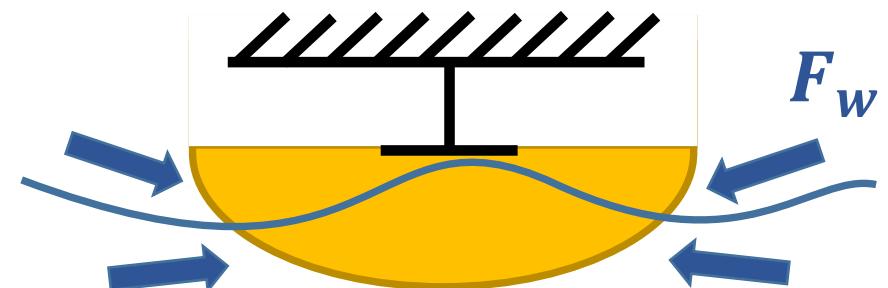
Hydrodynamic interactions – Potential flow

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$$\text{Time Domain: } (M - A_{\infty}) \ddot{X}(t) + \int_0^t h_r \dot{X}(t-t') \dot{X}(t) + KX(t) = F_w(t) + F_m(t) + F_g(t)$$

Radiation Forces

Froude-Krylov and Diffraction Forces



$$\text{Frequency Domain: } \{-\omega_w^2 [M + A(\omega_w)] + j\omega_w B(\omega_w) + K\} X(j\omega_w) = F_w(j\omega_w)$$

Hydrodynamic interactions – Potential flow

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Radiation Forces

Froude-Krylov and Diffraction Forces

$$\text{Frequency Domain: } \{-\omega_w^2 [M + A(\omega_w)] + j\omega_w B(\omega_w) + K\} X(j\omega_w) = F_w(j\omega_w)$$

- Linear Model
- Potential flow theory
- Frequency domain analysis
- No mooring forces

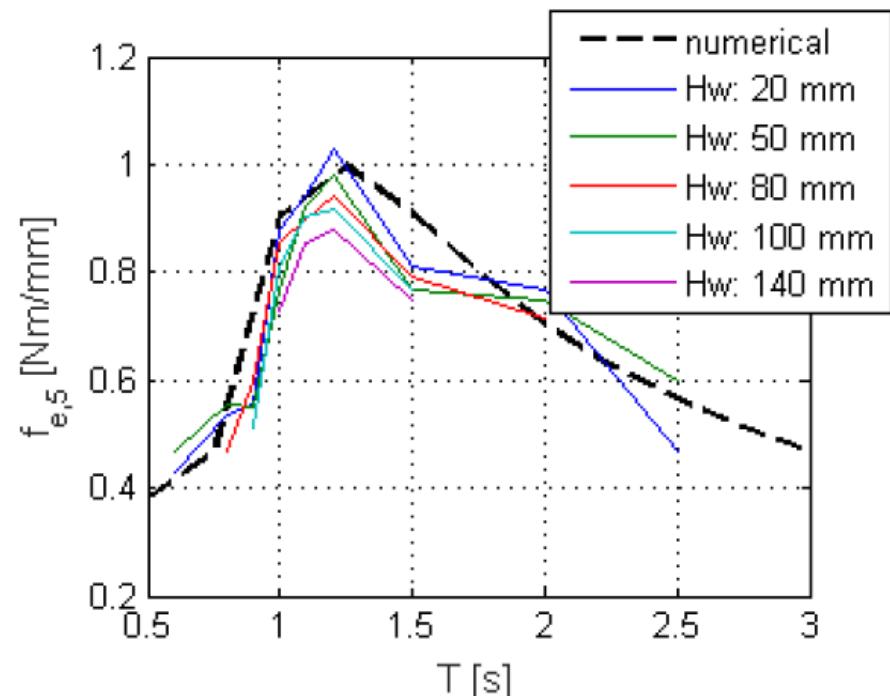
Model validation

Experimental test campaign @ Hydrodynamic and Maritime Research Centre of University College of Cork (HRMC)

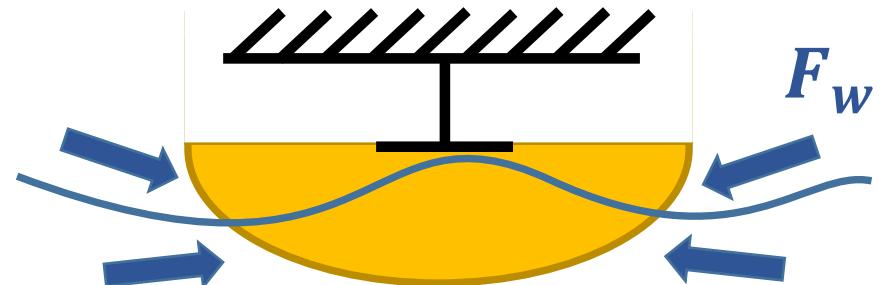
Hydrodynamic interactions – Potential flow validation

Experimental tests campaign in Cork

$$\{-\omega_w^2[M + A(\omega_w)] + j\omega_w B(\omega_w) + K\}X(j\omega_w) = F_w(j\omega_w)$$



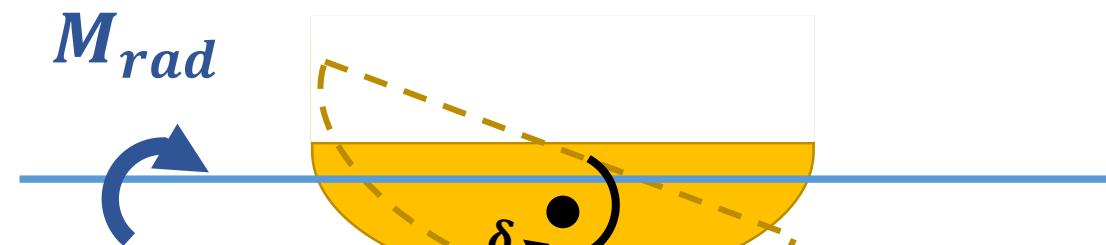
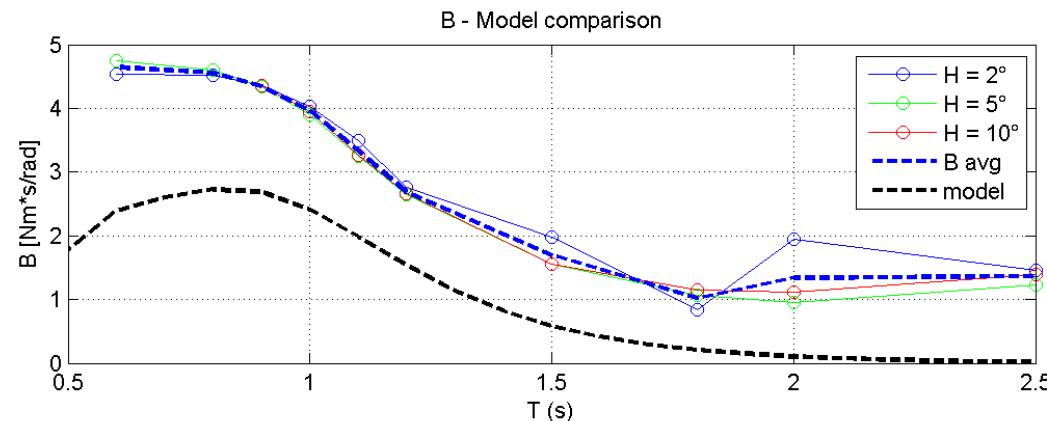
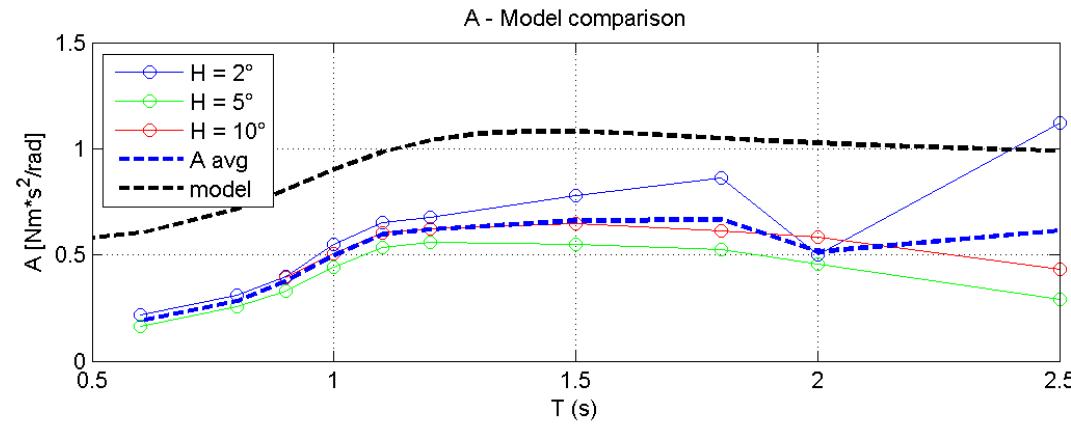
Wave Excitation Force coefficients – Froude-Krylov and Diffraction forces



✓ Good agreement

Hydrodynamic interactions – Potential flow validation

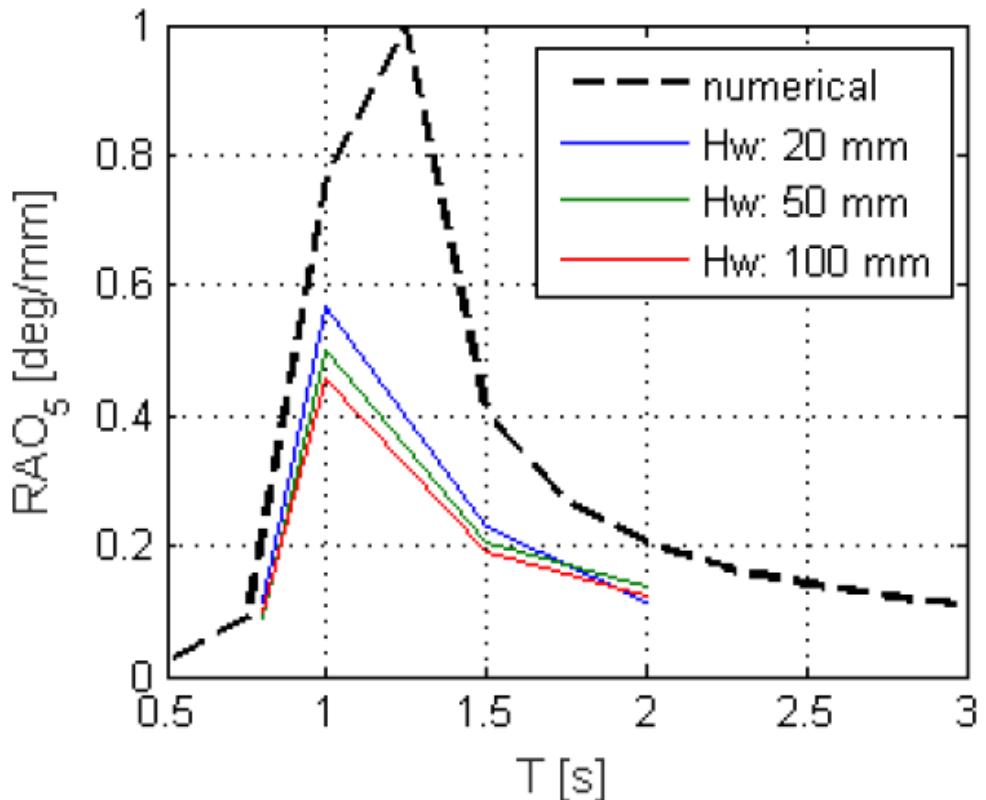
$$\{-\omega_w^2[M + A(\omega_w)] + j\omega_w B(\omega_w) + K\}X(j\omega_w) = F_w(j\omega_w)$$



✗ Bad agreement

Potential Flow Limits

Pitch Response Amplitude Operator (RAO)



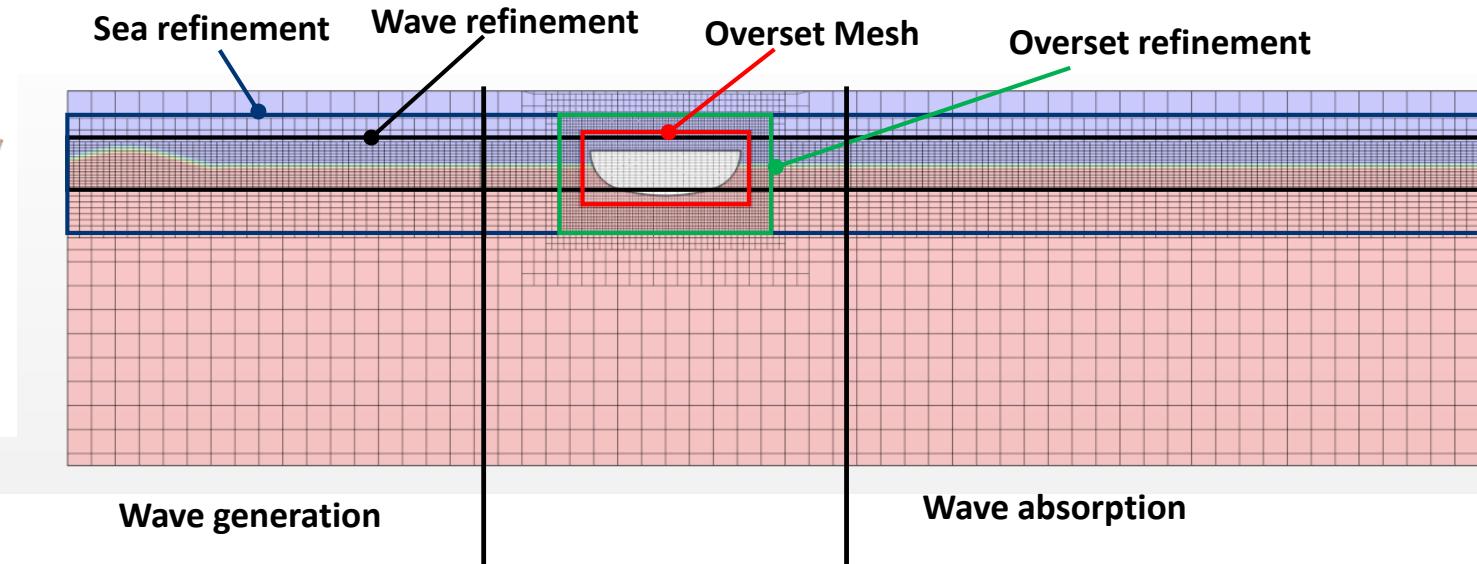
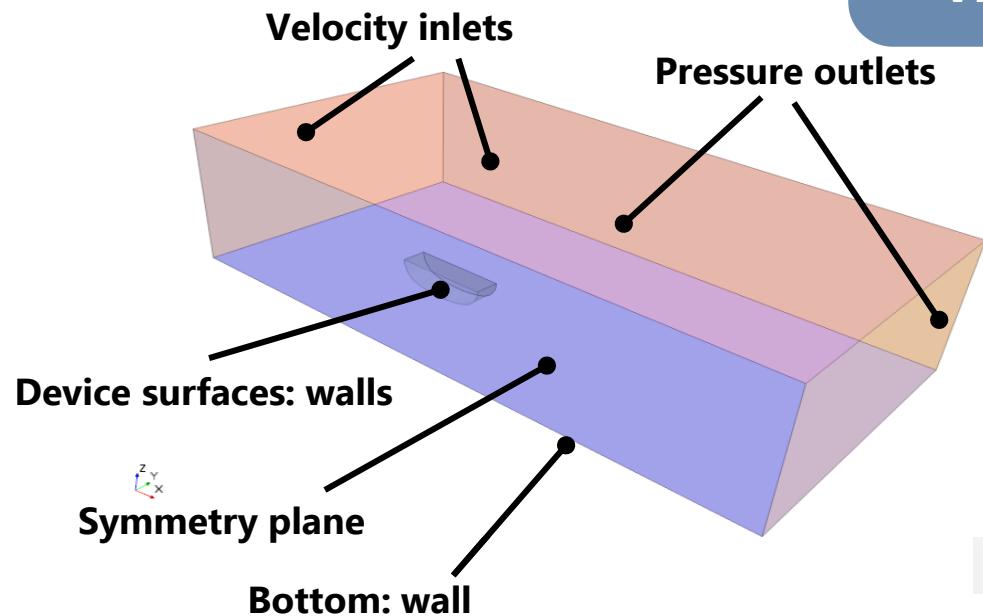
NOT CONSIDERED:

- Viscous Forces
- Instantaneous Wetted Surface

✓ More influent at higher amplitudes

CFD – Volume Of Fluid RANS in Star-CCM+

- Imposed Oscillatory Motion for Radiation Forces Identification
- Virtual Beach on the tank sides

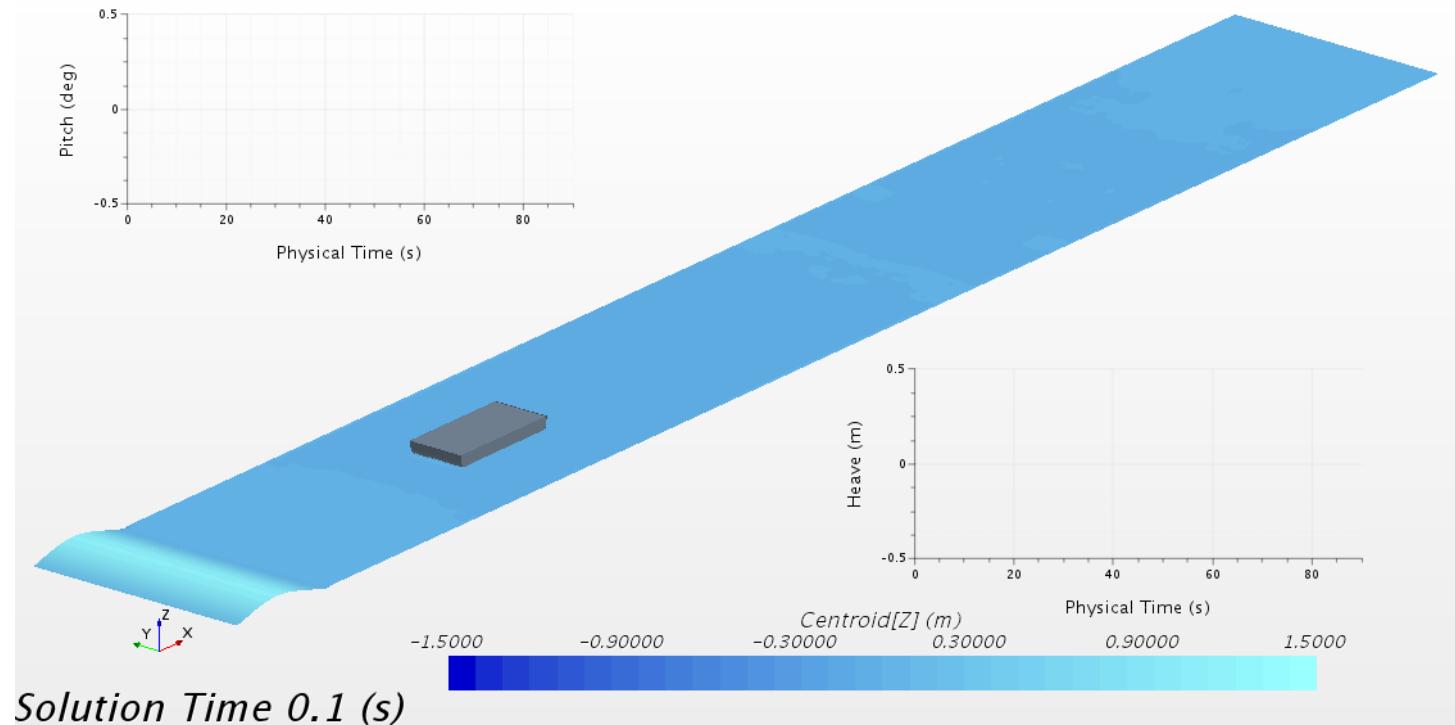
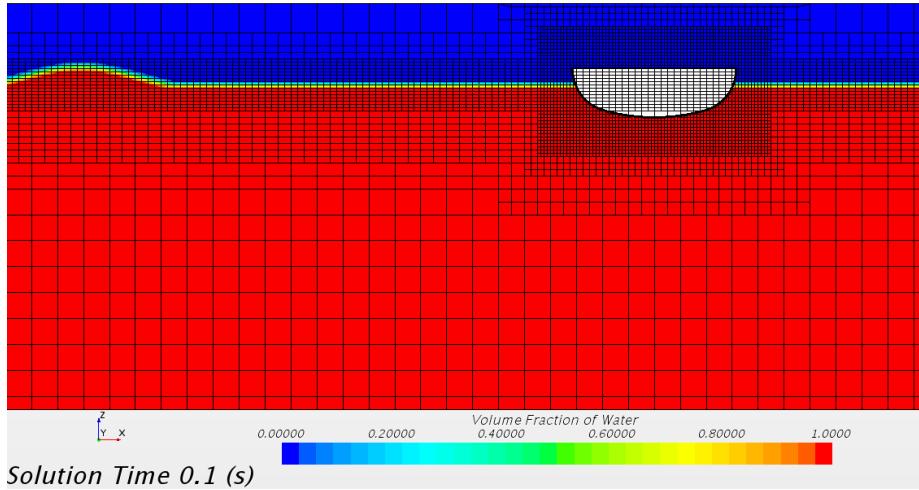


Calibration and Convergence analysis:

- Minimum computational domain

- Optimized mesh size
- Calibration on experimental and benchmark data

CFD – Volume Of Fluid RANS in Star-CCM+



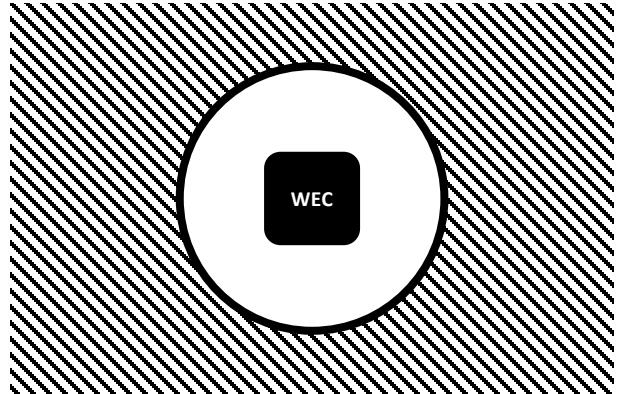
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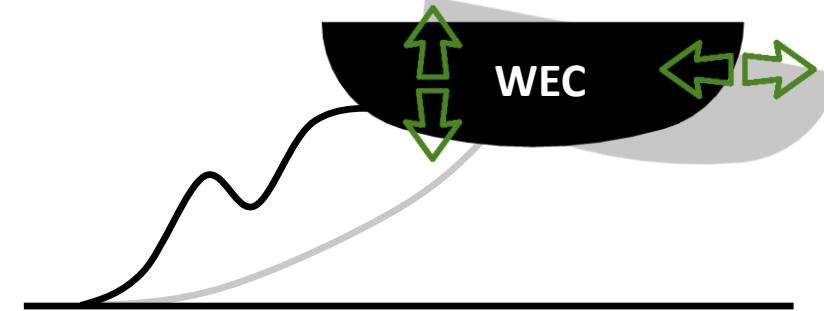
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Moorings requirements

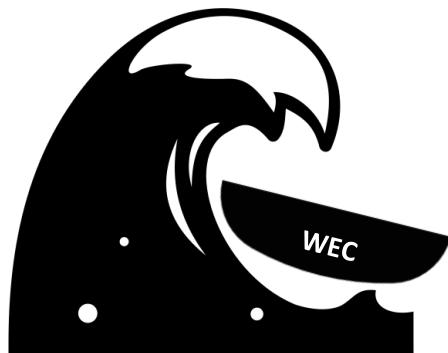
Station keeping



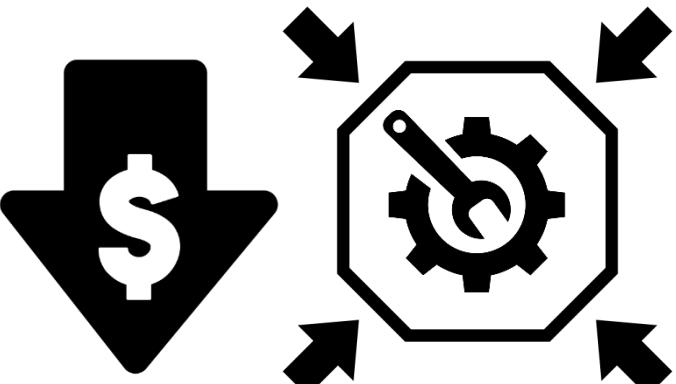
Compliance



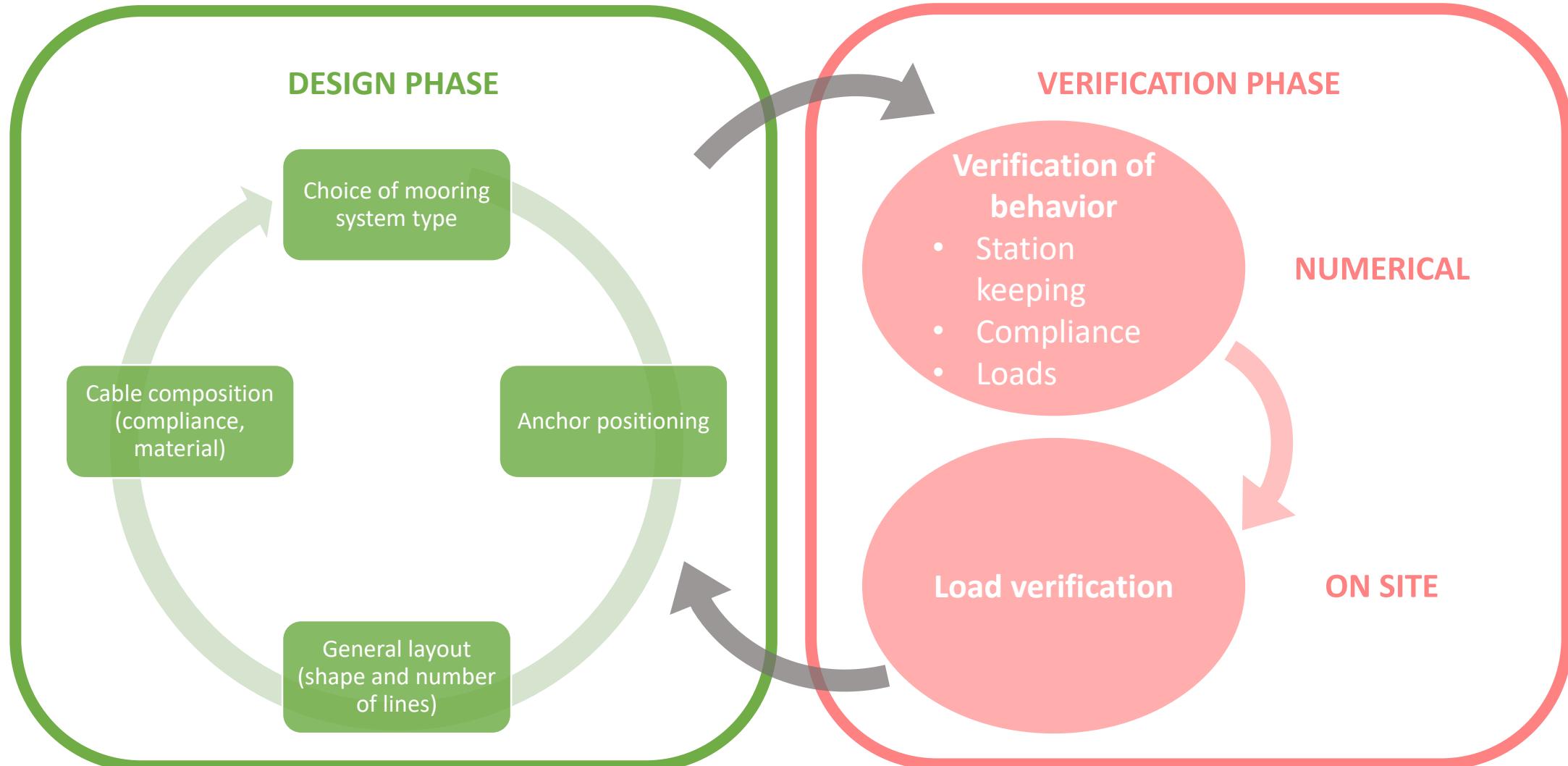
Survivability



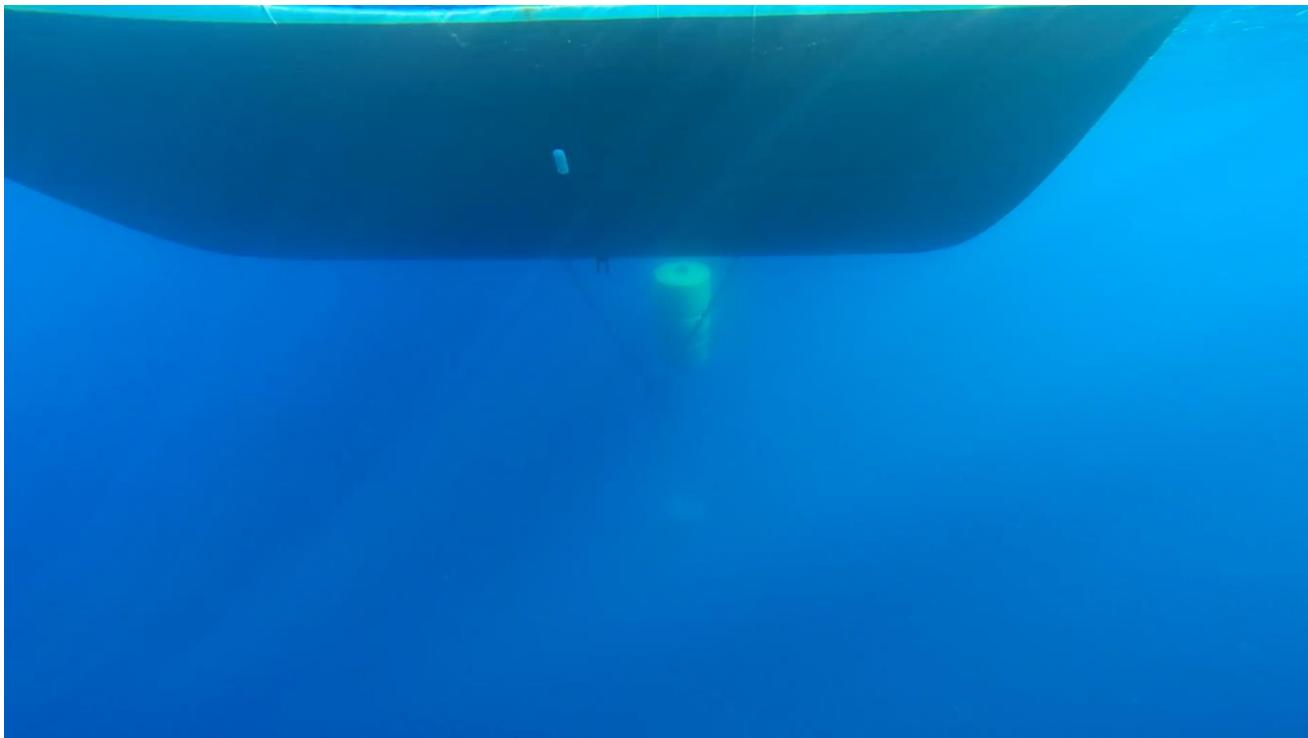
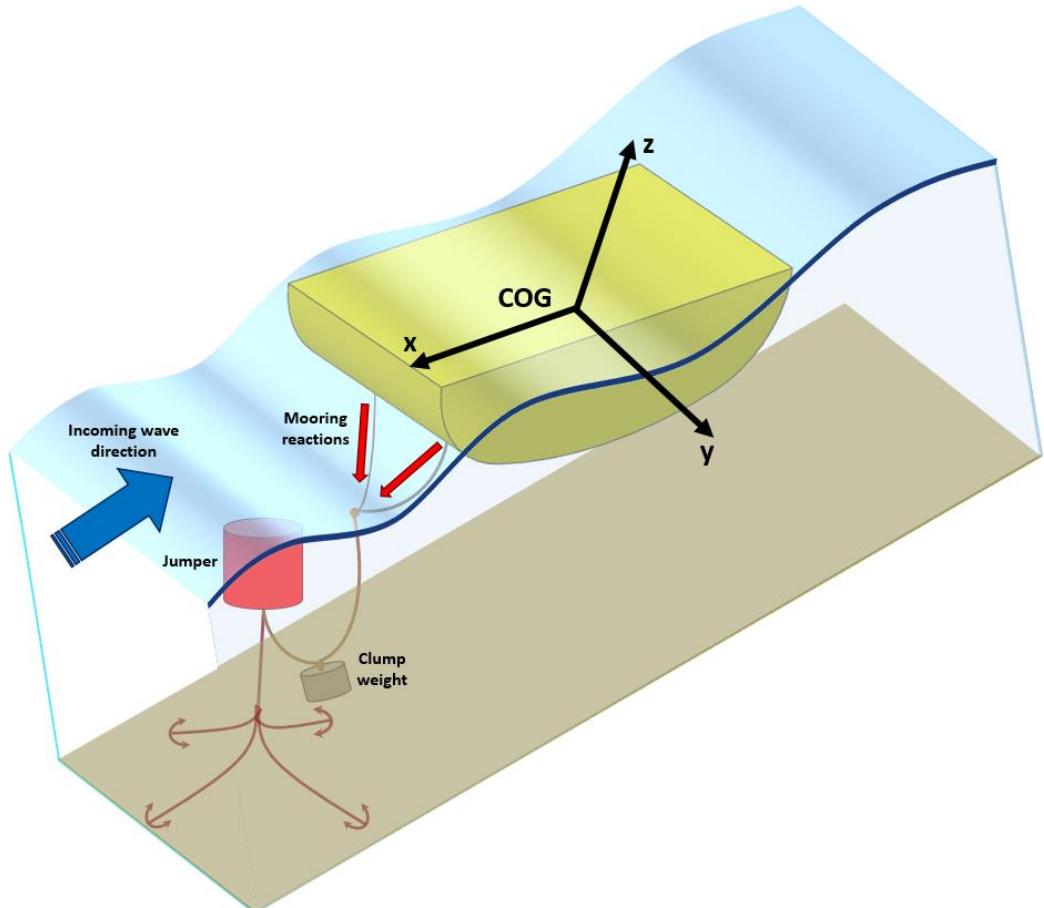
Low Maintenance



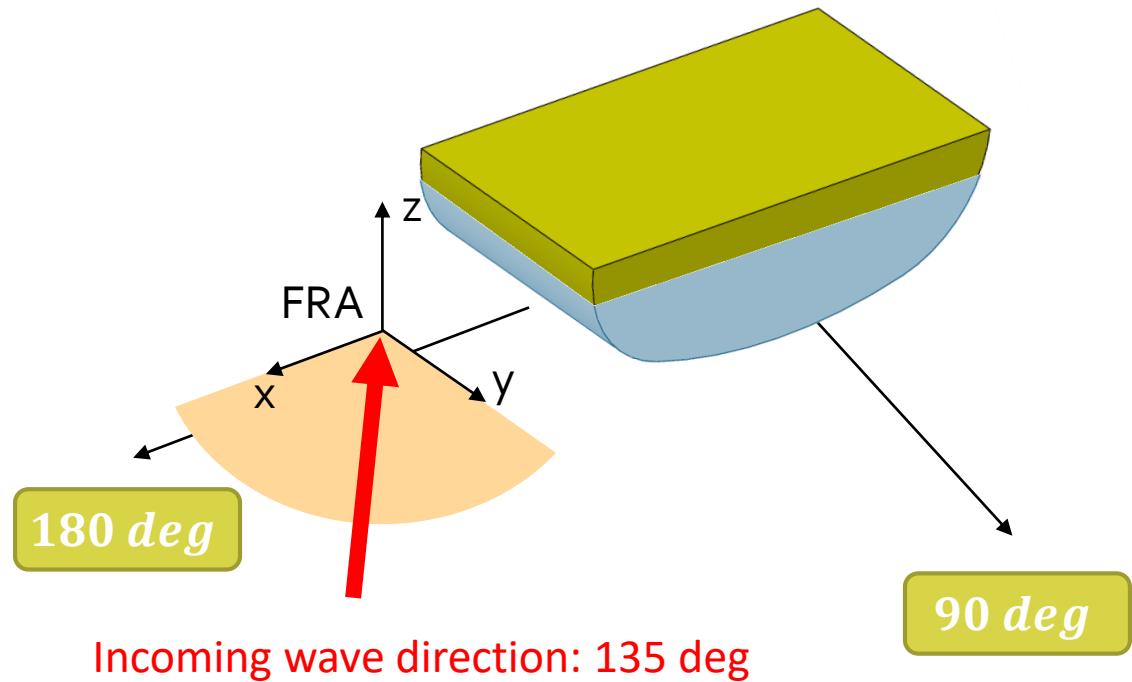
Moorings design and analysis



Starting point: Pantelleria Mooring system

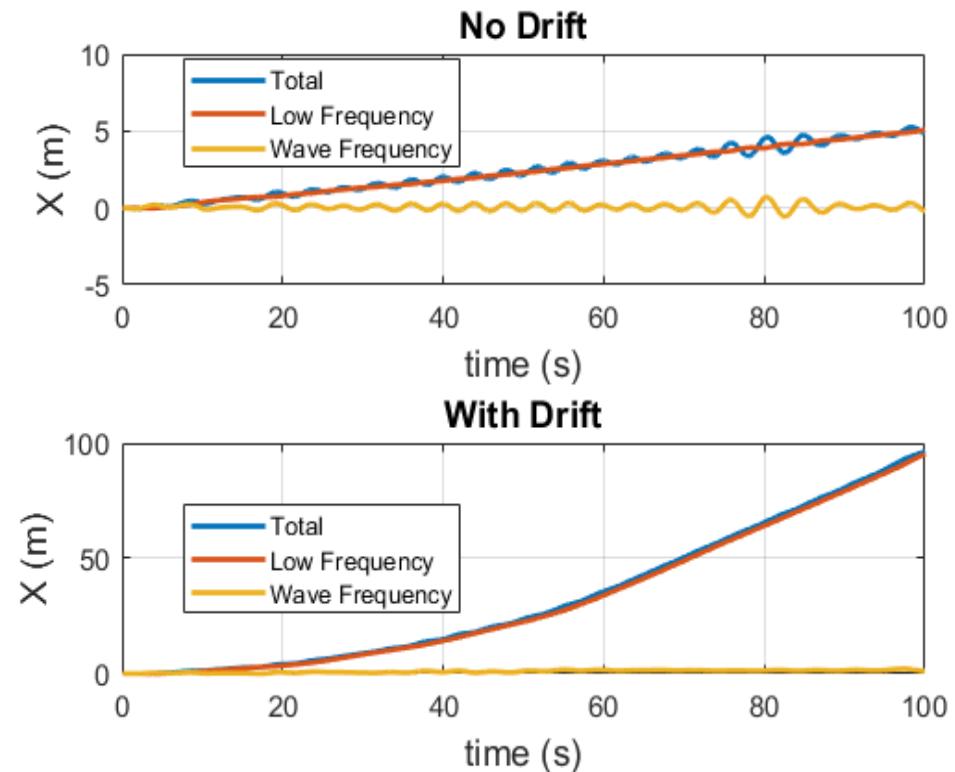
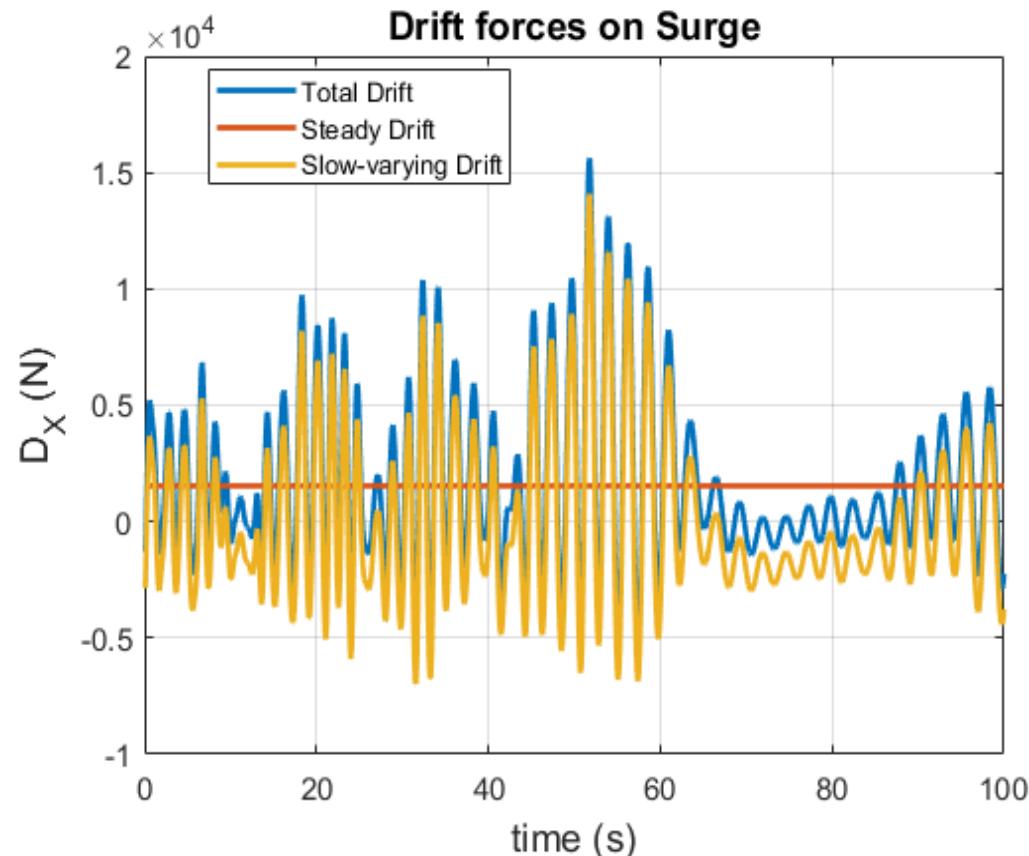


Starting point: Pantelleria Mooring system

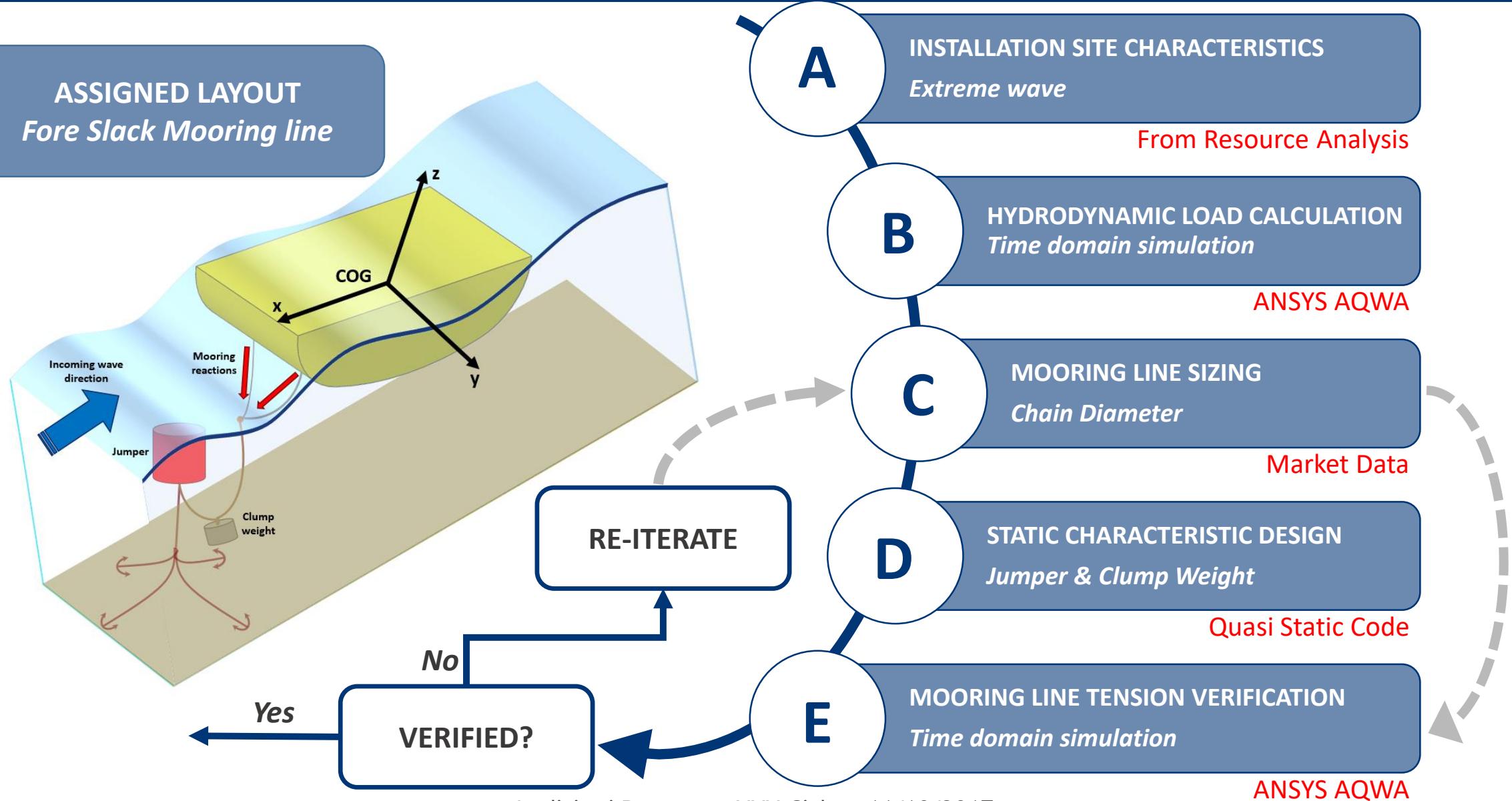


Importance of Drift Forces

Potential Flow Second Order effects



Mooring design workflow

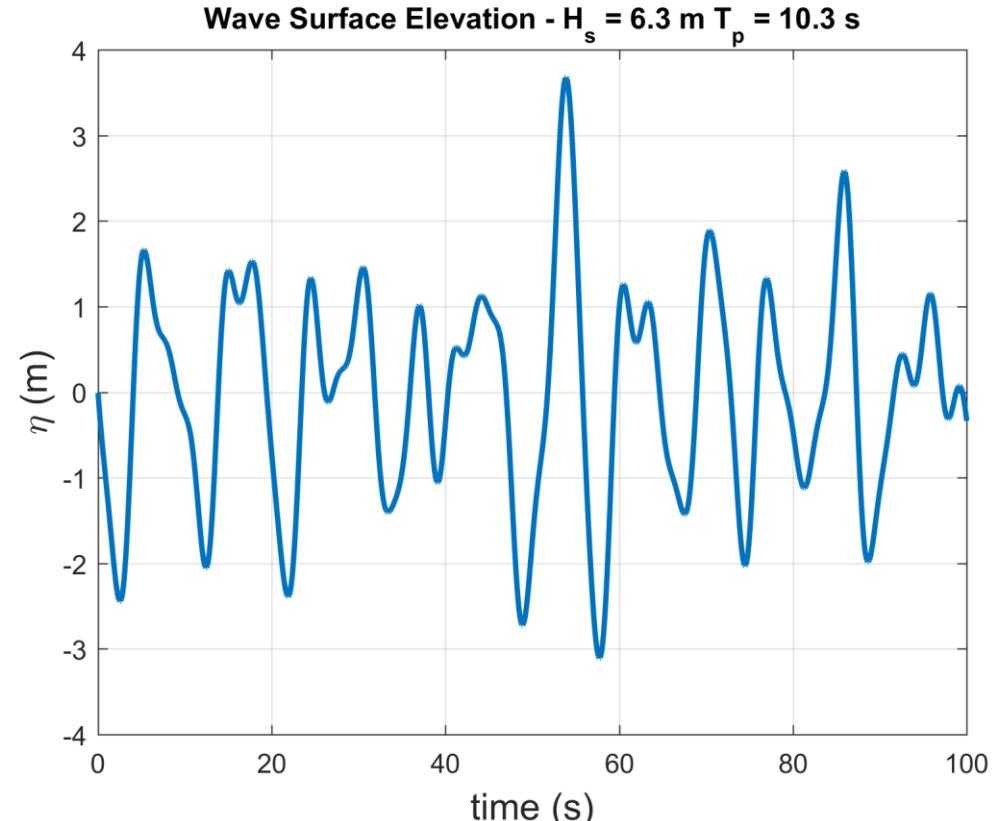
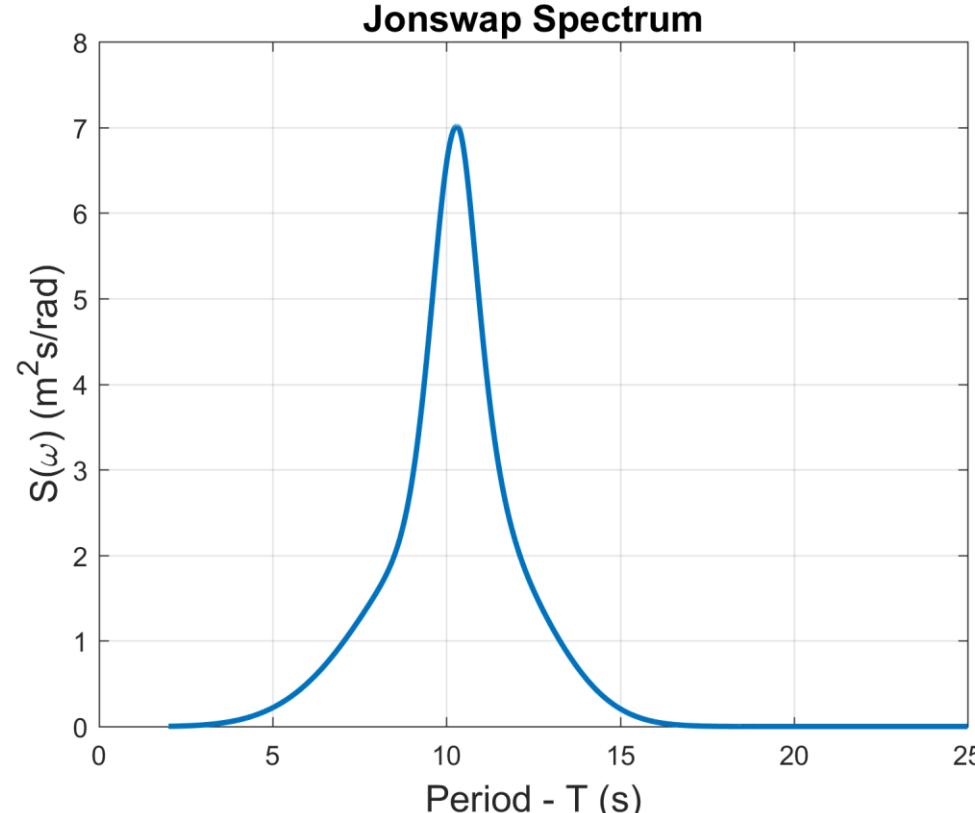


Significant Height	(m)	6.3
Peak Period	(s)	10.3
Simulation time	(s)	100

Secular wave properties

A

Irregular Wave Properties		
Significant Height	(m)	6.3
Peak Period	(s)	10.3
Simulation time	(s)	100

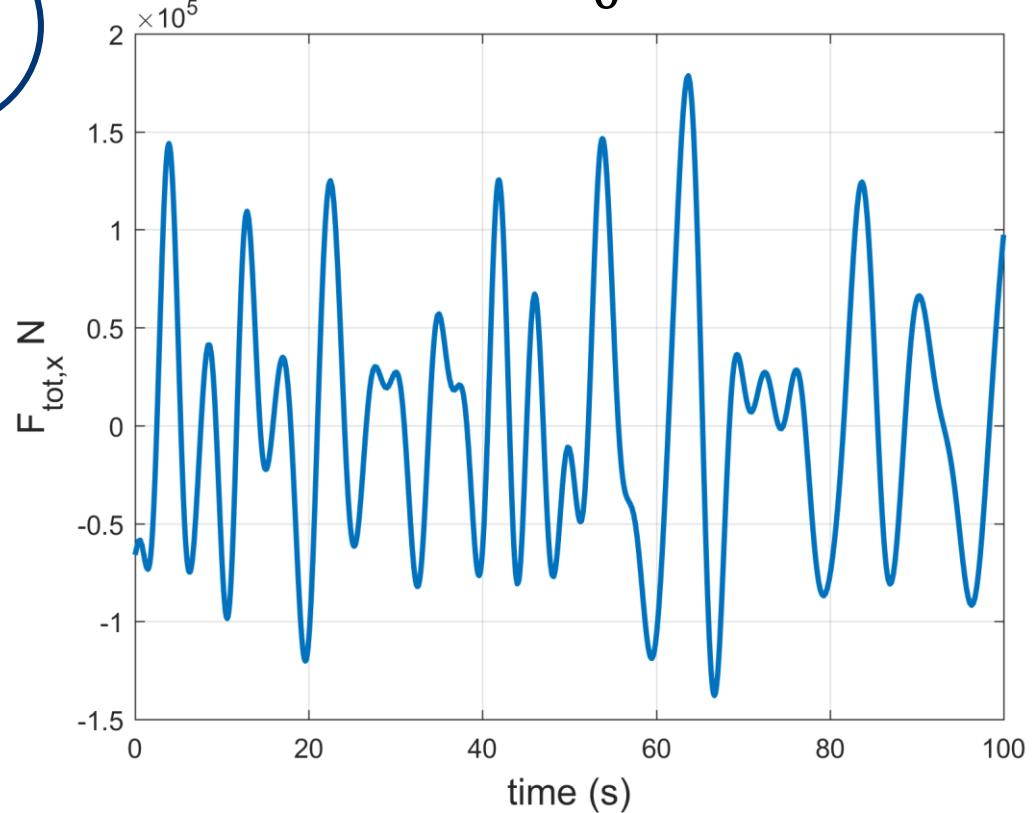


Hydrodynamic loads

Time domain with no moorings and no gyroscope (Surge DOF):

$$(M + A_\infty)\ddot{X} + \int_0^t h_r \dot{X}(t - t') \dot{X} dt' + KX = F_{FK} + F_{diffraction} + F_{drift}$$

B



$F_{tot,max} = 180 \text{ kN}$

Mooring line sizing

Chain properties from supplier catalogue

Mass per unit length	(kg/m)	14.8
Chain Diameter	(mm)	26
Equivalent Cross Sectional Area	(m ²)	0.0069
Axial Stiffness per unit length	(kN)	57730
Working Load	(kN)	278
Breaking Load (B.L.)	(kN)	389

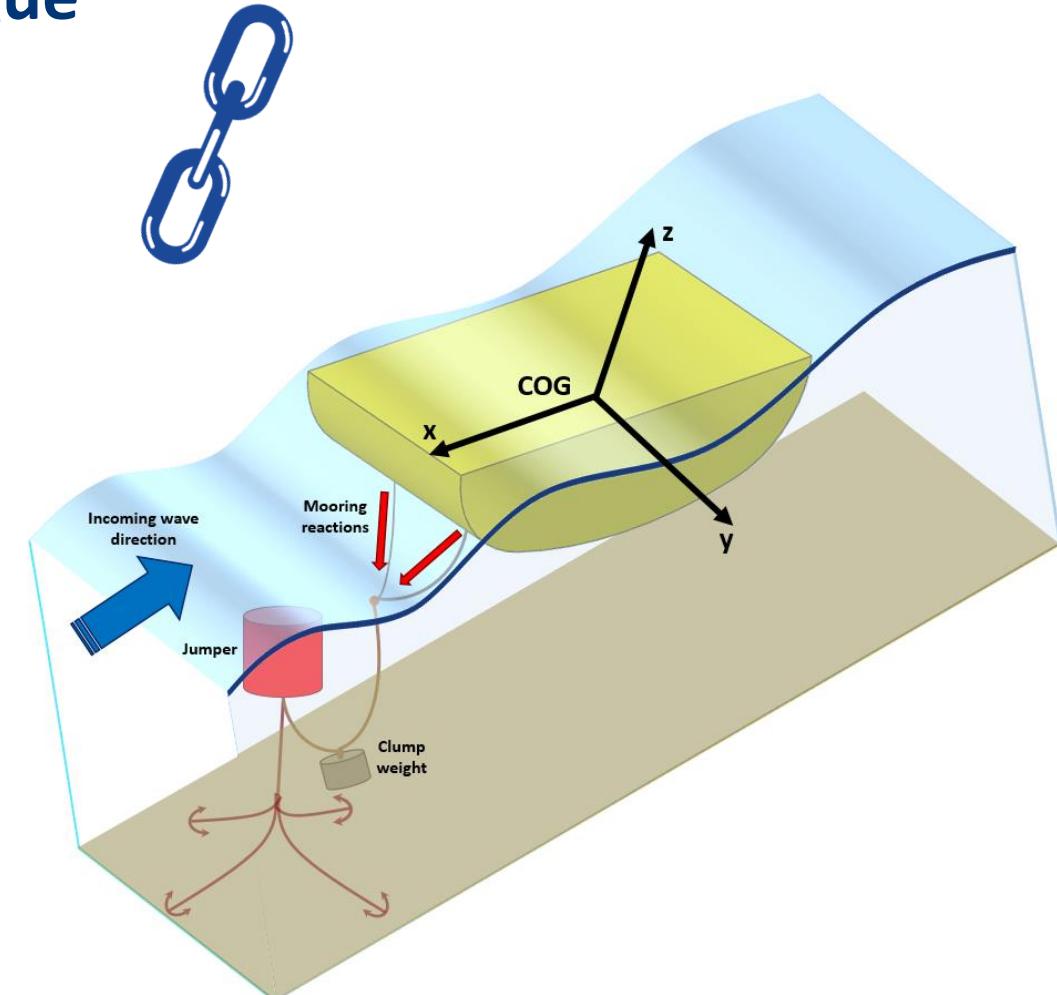
$$H = AE \sqrt{\left(\frac{T}{AE} + 1\right)^2 - \frac{2wZ}{AE}} - AE$$

$$X = \frac{H}{w} \sinh^{-1} \left(\frac{wL}{H} \right) + \frac{HL}{AE}$$

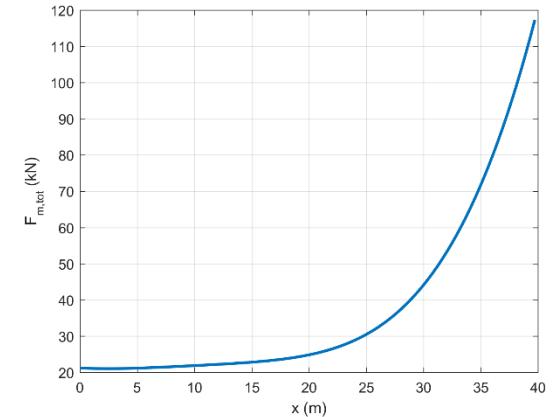
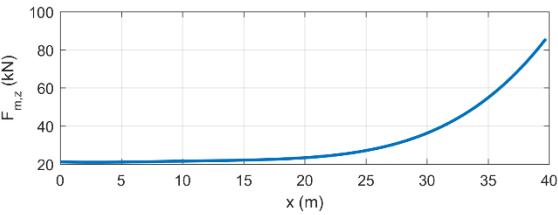
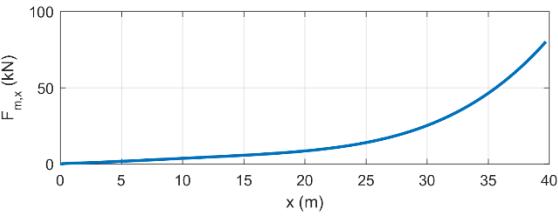
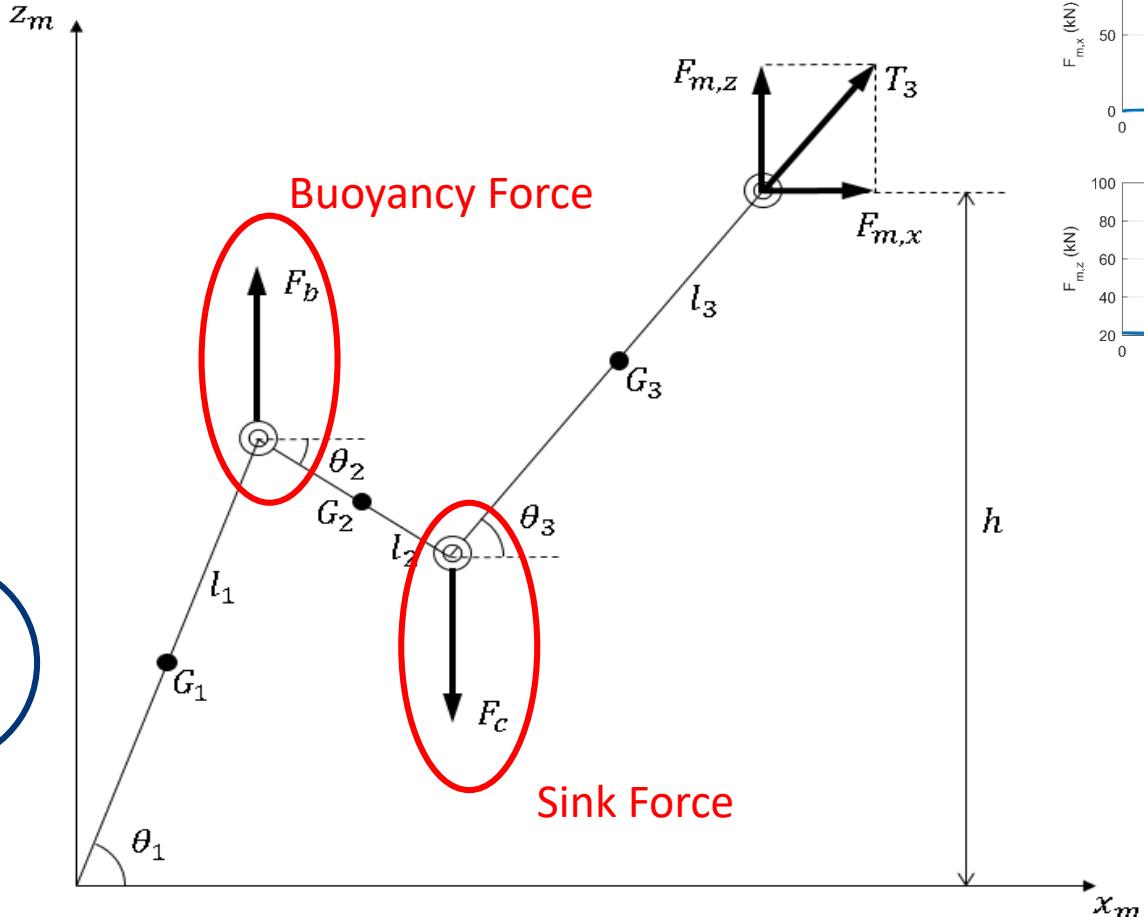
Iteration

$$V = wL$$

$$T = \sqrt{H^2 + V^2}$$



Static characteristic design



Design parameters

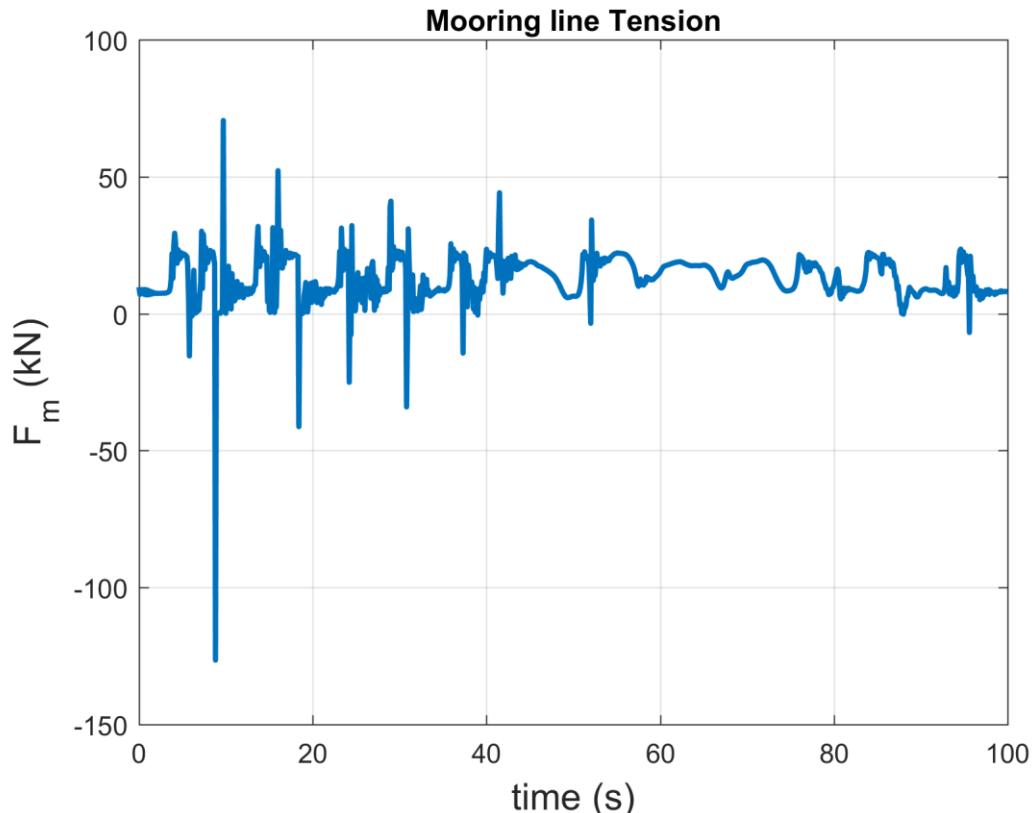
- Buoyancy Force
- Clump weight
- Lines lengths

GOALS

- ✓ Non-linear behavior
- ✓ Small loads

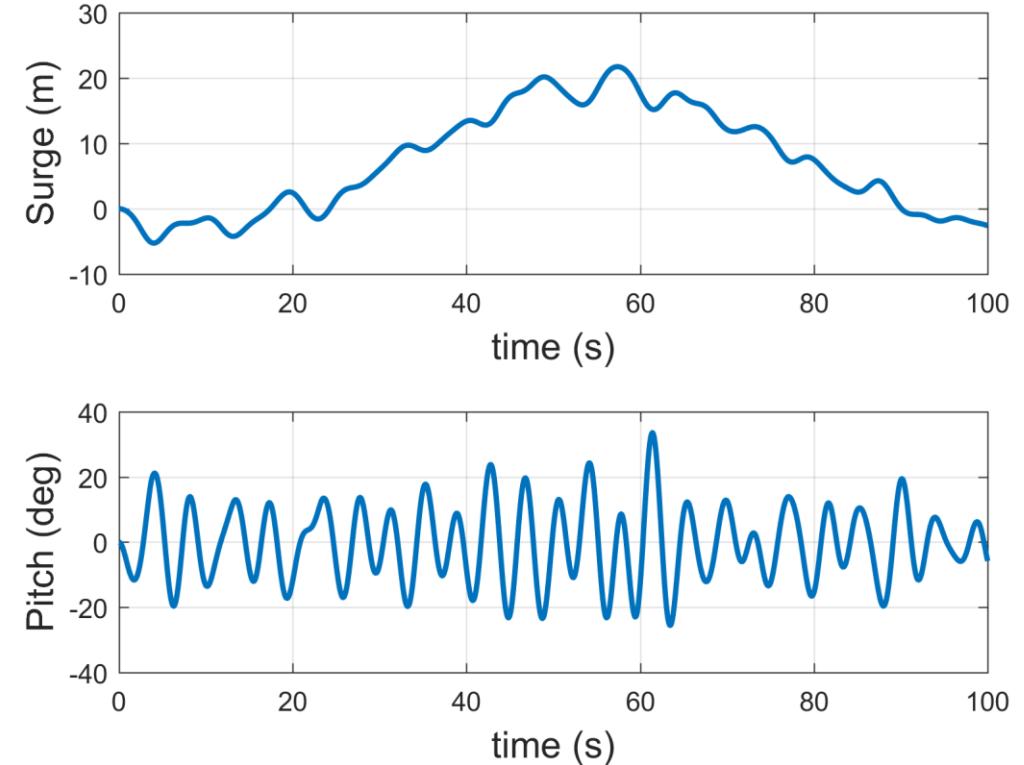
Mooring line tension verification

E



$$F_{m,max} = 126 \text{ kN}$$

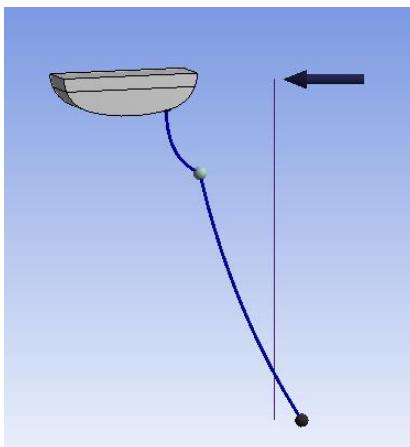
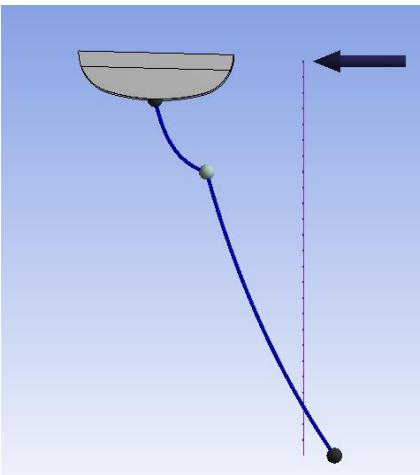
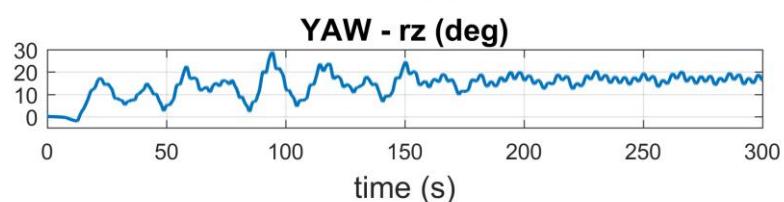
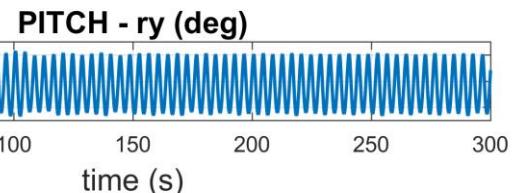
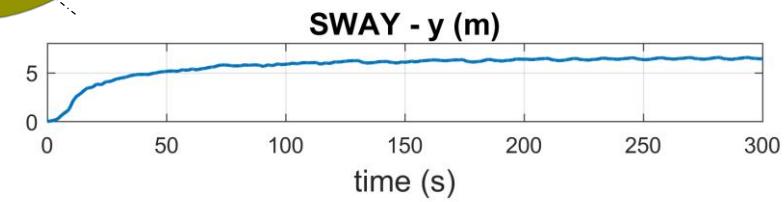
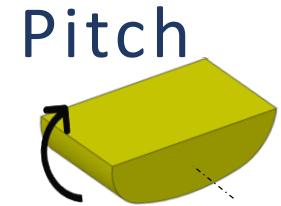
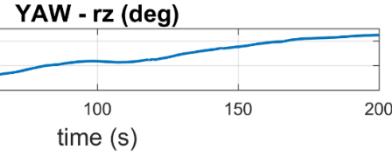
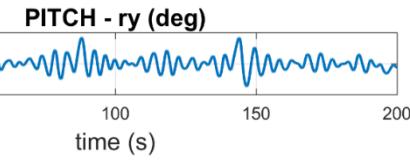
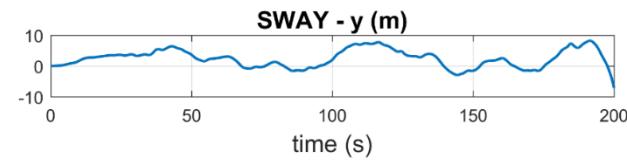
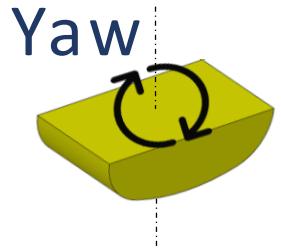
Floater dynamics with mooring actions



✓ Structural sizing verified with a safety factor of

$$B.L./F_{m,max} = 3$$

Weathervaning problem: wave and current



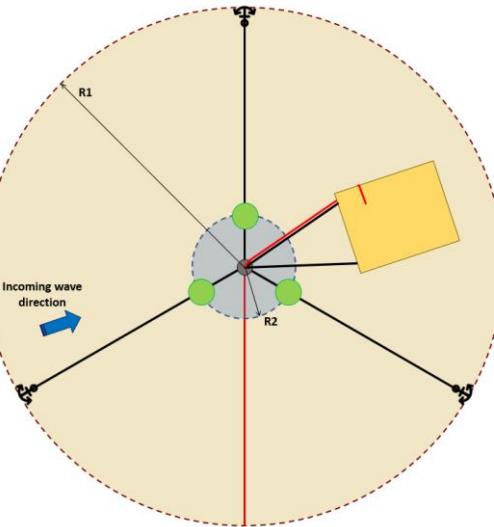
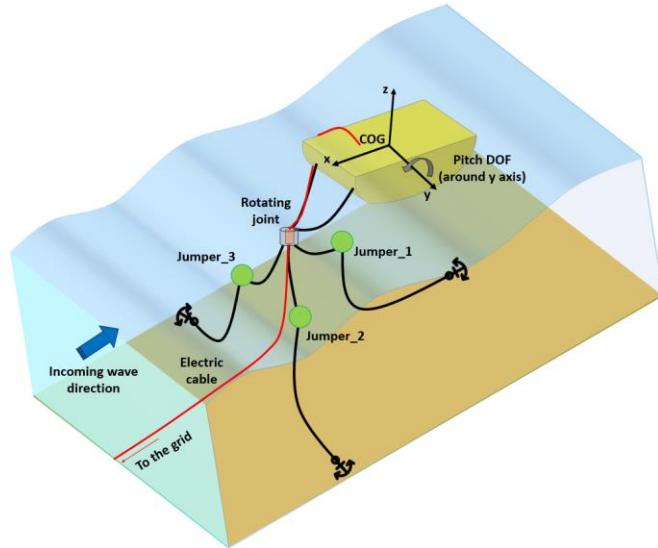
Central connection point

- ✓ Minimize mooring loads
- ✓ Best solution for joint connection
- ✗ Yaw and Sway motions diverge
- ✗ Pitch motion strongly irregular

Fore connection point

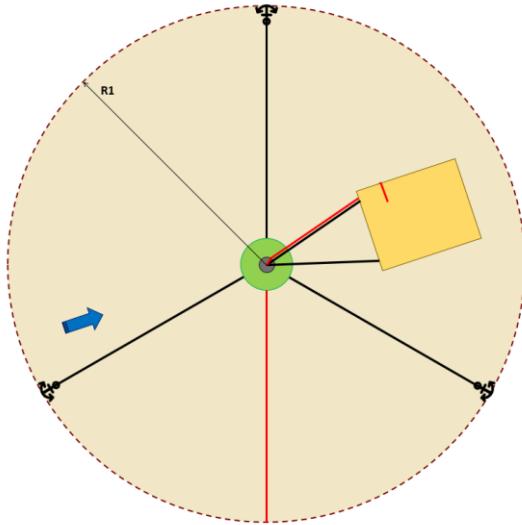
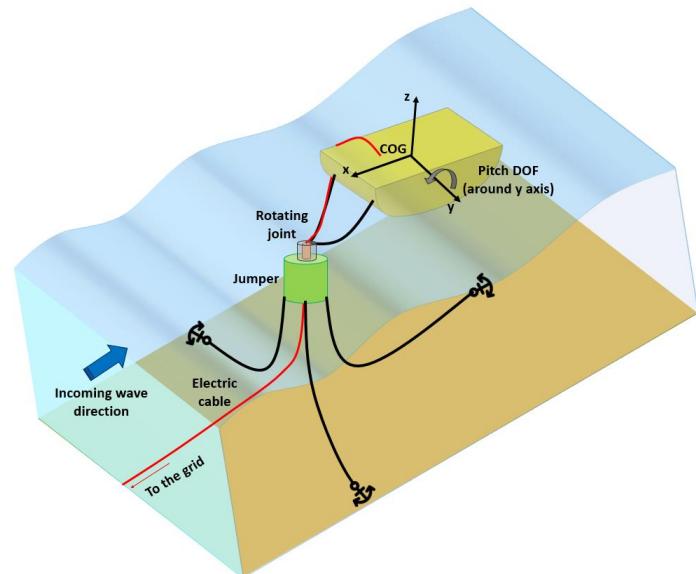
- ✓ Yaw and Sway motions stable
- ✓ Regular Pitch motion
- ✗ Higher mooring recall force
- ✗ More complex moorings layout

New moorings systems: grid connection & weathervane



Configuration 1

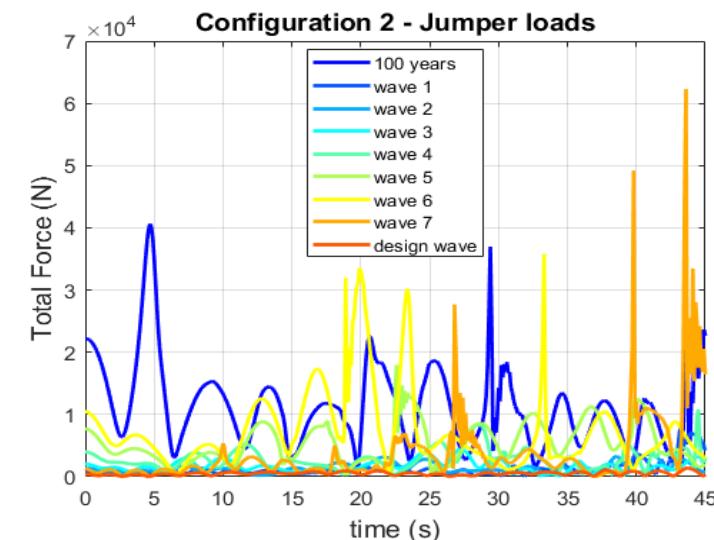
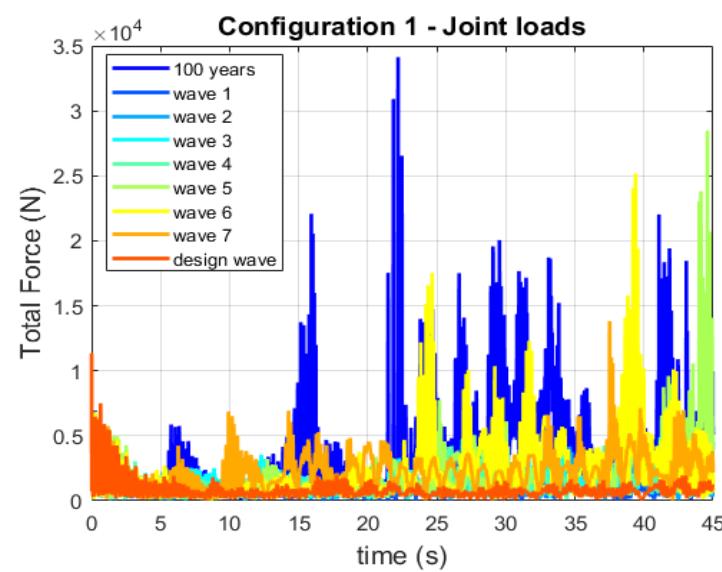
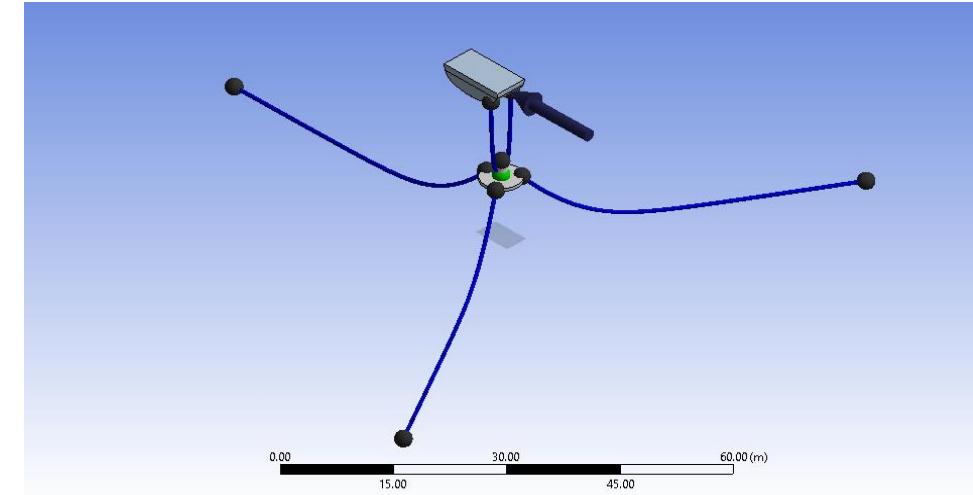
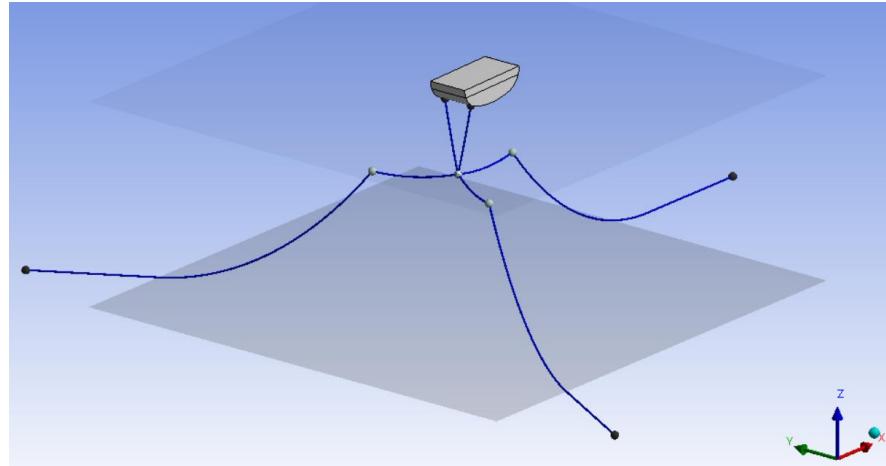
- 3 jumpers
- Free joint motion



Configuration 2

- Single jumper
- Joint follows the jumper

New moorings systems: grid connection & weathervane



Conclusions

- Numerical wave tank modelling
 - Possibility to run tests at reduced costs
 - Identification of non-linear phenomena involved in the floater-waves dynamics
 - 6 DoF simulations in irregular waves
- Mooring modelling and design
 - Wave to wire model expansion with 3 DoF quasi-static modelling
 - Modelling of dynamic mooring system with multiple lines
 - Design of slack mooring systems for floating WECs



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DI TORINO

Thank you